

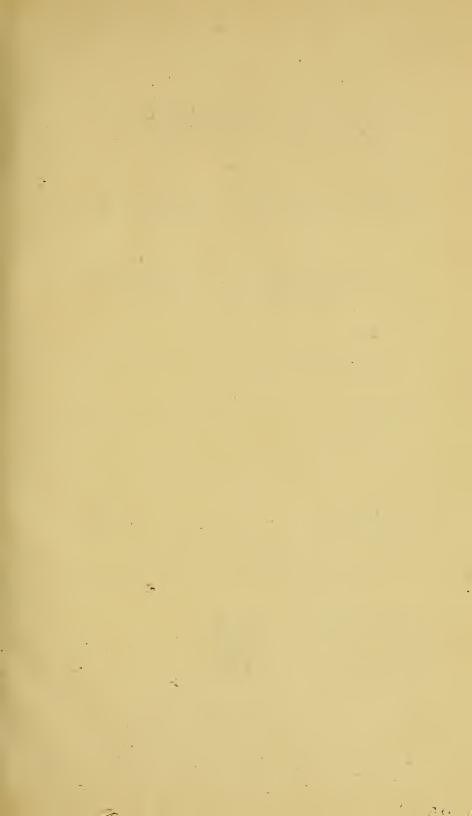
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COMPLETE KEY

TO

GUMMERE'S SURVEYING;

IN WHICH

THE OPERATIONS OF ALL THE EXAMPLES NOT SOLVED IN THAT WORK ARE EXHIBITED AT LARGE.

PRINCIPALLY DESIGNED

TO FACILITATE THE LABOUR OF TEACHERS.

AND TO ASSIST THOSE

WHO HAVE NOT THE OPPORTUNITY OF THEIR INSTRUCTION.

By SAMUEL ALSOP.

ADAPTED TO THE REVISED EDITION OF THE SURVEYING

By ISAAC SHARPLESS,

AUTHOR OF "A TEXT-BOOK OF GEOMETRY AND TRIGONOMETRY."





PHILADELPHIA:
PORTER & COATES.

1884

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KEY

TO

GUMMERE'S SURVEYING.

PLANE TRIGONOMETRY.

CASE 1. Example 3. (Pl. 1, fig. 1.) Angle C=180°—A—B=46° 15'. As sin. A 79° 23' - Ar. Co. 0.007499 Is to sin. B 54° 22' 9.909963 So is BC 125 2.096910 To AC 103.4 Again, - - - Ar. Co. 0.007499 As sin, A -Is to sin. C 46° 15' - -9.858756 So is BC -To AB 91.87 Example 4. (Pl. 1, fig. 2.) Angle C=90°-A=33° 12'. As sin. C 33° 12' - - Ar. Co. 0.261566 Is to sin. B 90 - - 10.000000 So is AB 53.66 -To AC 98 Ar. Co. 0.261566 As sin. C - -Is to sin. A 56° 48' -9,922603 So is AB -1.729651

To BC 82

_ 1.913820

Example 5. (Pl. 1, fig 2.)

Angle	C=9	00°—A	1=	50°	50'.

									0.199573
								**************************************	10.000000
So is BC 407.37	•	-	-	•	-	-	-		2.609989
To AC 645	-	-	-	-	-	-	-		2.809562
As sin. A		-	_	_	-	-	_	Ar. Co.	0.199573
As sin. A Is to sin. C 50° 50′									
	-	•	-	-	-	-	-		9.889477

		OAS	SE 2.	•		
	Ехамр	LE 3.	(Pl.	1, fig. 1	l .)	
As AC 306 -					Ar. Co.	7.514278
Is to AB 274						2.437751
So is sin. B ·	78° 1	3' -				9.990750
To sin. C	61 1	4 -				9.942779
	139 2	7				
	180			,		
		_				
A	40 3	3 =				
As sin. B 78°	3' -				Ar. Co.	0.009515
Is to sin. A 40	° 23′					9.812988
So is AC 306						2.485721
To BC 203.4						2.308224
	Ехамі	PLE 4.	(Pl.	1, fig. 2	2.)	7
As AC 272 -					Ar. Co.	7.565431
Is to AB 232						2.365488
So is sin. B -	90°					10.000000

9.930919 To sin. C - - 58° 32'

A - - 31° 28'

Is to sin. A 31° 28′	0.000000 9.717673 2.434569
To BC 142	2.152242
Example 5. (Pl. 1, fig. 2.)	
As AC 150 Ar. Co.	7.823909
	1.838849
	10.000000
To sin. A - 27° 23'	9.662758
C - 62° 37′	,
	0.000000
As sin. B Ar. Co. Is to sin. C 62° 37′	9.948388
So is AC	2.176091
To AB 133.2	2.124479
·	
CASE 3.	
CASE 3.	
Example 2. (Pl. 1, fig. 3.)	
Example 2. (Pl. 1, fig. 3.)	
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} 15^{\circ}$	
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} 15'$ As AB+BC 185 Ar. Co.	
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} 15'$ As AB+BC 185 Ar. Co. Is to AB-BC 33	1.518514
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} \ 15'$ As AB+BC 185 Ar. Co. Is to AB-BC 33 So is tang. $\frac{C+A}{2}$ 39° 15'	
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} 15'$ As AB+BC 185 Ar. Co. Is to AB-BC 33	1.518514
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} \ 15'$ As AB+BC 185 Ar. Co. Is to AB-BC 33 So is tang. $\frac{C+A}{2}$ 39° 15'	1.518514 9.912240
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} 15'$ As AB+BC 185 Ar. Co. Is to AB-BC 33 So is tang. $\frac{C+A}{2}$ 39° 15' To tang. $\frac{C-A}{2}$ 8° 18' $\frac{C-A}{47^{\circ} 33'}$	1.518514 9.912240 9.163582
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} 15'$ As AB+BC 185 Ar. Co. Is to AB-BC 33	1.518514 9.912240 9.163582
Example 2. (Pl. 1, fig. 3.) $\frac{A+C}{2} = \frac{180^{\circ} - B}{2} = 39^{\circ} \ 15'$ As AB+BC 185 Ar. Co. Is to AB-BC 33	1.518514 9.912240 9.163582 0.288792

Example 3. (Pl. 1, fig. 2.)

C	+	\mathbf{A}_{\perp}	= 18	0°—	-B	1	50	
	2			2		4	.0	
As AB+BC 1677	-	-	-	-	-	-	-	Ar. Co. 6.775467
Is to AB—BC 103	-	-	-	-	-	-	-	2.012837
So is tang. $\frac{C+A}{2}$						-	-	10.000000
To tang. $\frac{C-A}{2}$	-	-	3°	31′		-	-	8.788304
C	-	-	48°	31	,			
					-			
			-	•	-	-	-	Ar. Co. 0.178878
Is to sin. B 90 -	•	-	-	-	-	-	-	10.000000
So is BC 787 -	•	-	-	-	-	-	-	2.895975
To AC 1188 -	-	-	_	-	-	-	-	3.074853

CASE 4.

Rule 2.

Example 2. (Pl. 1 fig. 4.)

AC 47 AB 64 Ar. Co. 8.193820 BC 34 Ar. Co. 8.468521 2)145

Half sum 72.5 - - - - 1.860338

Difference 25.5 - - - - 1.406540

2)19.929219

Cos. ½ B 22° 49′ - - - 9.964609

B 45° 38′

Example 3. (Pl. 1, fig. 4.)

AB 108
BC 54 Ar. Co. 8.267606
AC 88 Ar. Co. 8.055517

2)250

Half sum 125 - - - - 2.096910

Difference 17 -- - - 1.230449

2)19.650482

Cos. ½ C 48° 2' - - 9.825241 C 96° 4'

RIGHT ANGLED TRIANGLES.

First Method.

Example 2. (Pl. 1, fig. 5.)

Making AC radius, CB is sine of A, and AB is cos. A; hence,

As radius	s - -	-	_	_	_	_	_	_	_	A	r . C	lo.	0.000000
Is to sin.	A 27°	46	_	_	_	_	_	_	_	_	_	_	9.668267
So is AC			_	_	_	_	-	_	_	_	_	_	1.563125
													4.004.000
To BC 1	7.04	-	-	-	-	-	-	-	-	-	-	-	1.231392
And,													
As radiu	a									A	r (٠ <u>,</u>	0.000000
Is to cos.	_	-	_		Ē	_		Ū	Ī	23.			9.946871
So is AC		•	•	Ī		-	_	-	Ī	Ī	Ī	Ī	1.563125
SO IS AC	,	-	Ī	-	_	_	-	Ī	Ī		_	Ī	1.500125
To AB	32.36	-	-	-	-	-	-	-	-	-	-	-	1.509996
		77			_	/T				_ 、			
		Eix	KAM	PLE	E 3.	(1	1.	l, f	ıg.	5.)			
Making AC	radiv	ıs, V	ve	ha	ve (CB	th	e s	ine,	an	d A	lΒ	the cosine of
A; hence,													
As sin. A	42° 9	1	-	-	-	-	-	-	-	A	r. (Co.	0.173230
Is to rad	ius -	-	•	-	-	-	-	-	-	-	-	-	10.000000
So is BC	193.6	-	-	-	-	-	-	-	-	-	-	-	2.286905
To AC	000 5												2.460135
10 AC 2	6.553	-		-	-	-	-	-	-	-	-	•	======
And,													
As sin. A		-	-	-	-	-	-	-	-	A	r. C	o.	0.173230
Is to cos.	A -	_	-	-	-	-	-	-	-	-	-	-	9.870047
So is BC		-	_	-	-	-	-	-	-	-	-	-	2.286905
m. And	2100												0.990199
To AB 2	213.9	-	-	-	-	-	-	-	-	-	-	-	2.330182
		$\mathbf{E}\mathbf{x}$	AM	PLI	z 4	. (]	P1.	1. f	ig. (6.)			
Making the	haza A								_		n 010	nt.	of A; making
AC the radius												ш	or A, making
		V 0 1	ردد	DIII	5 00	,SIII	0.0.	1 13	., .			α.	0.990407
As AB 46		-	-	-	-	-	-	-	-		Ar.	Co	. 8.330497 1.762679
Is to BC		-	-	-	-	-	-	-	-		-	-	10.000000
So is rad.			-	-	-	-	-	-	-		_		
To tang.	A 51° (3′	-	-	-	-	-	-	-		_	-	10.093176
And,													
As cos. A		-	-	-	-	-	-	-	-		Ar.		. 0.202066
Is to rad.		-	-	-	-	-	-	-	-		-	-	10.000000
So is AB		-	-	-	-	-	-	-				-	1.669503
To AC 7	4.4 -	-	-	-	-	-	-		-			-	1.871569

Second Method.—By Logarithms.

EXAMPLE 3.

•							
Hypothenu Base -		03 21					
Sum	7	24 -			log.	2.85	9739
Difference	:	82 -		-	- "	1.91	3814
					2))4.77	3553
Perpendicu	lar 243	3.65	•		-	2.38	6776
	E	KAMI	PLE 4	ŀ.			
Perpendicular	27.2 -	- ,	-	log.	1.43	4569 ——	
						9138	
Base	31.04	-		-	1.49	$\frac{1922}{}$	1.491922
	23.835	-	•	· -	1.37	7216	
	54.875			-	-		1.739374
							2)3.231296
Hypothenuse	41.27	-		-	-		1.615648

APPLICATION OF PLANE TRIGONOMETRY TO THE MENSURATION OF DISTANCES AND HEIGHTS.

Example 1. (See fig. 54, Surveying.)

Angle C=180°-A-B=56° 23'.

To find AC:

As sin. C 56° 23' -	-	-	-	-	-	•	Ar. (o.	0.079480
Is to sin. B 49° 23' -									
So is AB 500 yards	-	-	-	-	-	-		-	2.698970
To AC 455.8	-	-	-	-	-	-		_	2.658739

To find BC:											
As sm. C	-		_	_	_	_	-	A	r. (Co.	0.079480
Is to sin. A 74	° 14′	-	-	-	-	-	-	-	-	-	9.983345
So is AB	-		-	-	-	-	-	-	-	-	2.698970
To BC 577.8	-		-	-	-	-	-	-	-	-	2.761795
E	XAMP:	LE 2.	(F	ig.	55,	Su	rve	yın,	g.)		
As BC+AC	1575	-	-	-	-	-	-	A	r. (Co.	6.802719
Is to BC—AC			-	-	-	-	-	-			2.021189
So is tang. A-	~	62°	10′	-	-	-	-	-	-	-	10.277379
To tang. $\frac{A-B}{2}$	3	7°	12'	-	-	-	-	-	-	-	9.101287
		54°	58'								
As sin. B	-		_	_	_	-	_	A:	r. C	lo.	0.086813
Is to sin. C 55°	40'		-	-	-	-	-	-	_	-	9.916859
So is AC 735	-		-	-	-	-	-	-	-	-	2.866287
To AB 741.2	-	- -	-	-	-	-	-	-	-	-	2.869959
E	XAMP	LE 3.	(F	ig.	56,	Su	rve	yin	g.)		
Angle	CAL)=18	80—	-AI	OC-	—A	CI)=	31°	10)′
To find AC:											
As sin. CAD 3	1° 10	0' -	-	-	-	_	-	A	r. (o.	0.286065
Is to sin. ADC	53°	30′	-	-	-	-	_	_	-	_	9.905179
So is CD 300	-		-	-	-	-	- "	-	-	-	2.477121
To AC 465.98	-		-	-	-	-	-	-	-	-	2.668365
Angle	CDT)16	0.0	DC	T)	D	DC	۱_ (ഹം	EE	,
	ODL	IC	,,,	JJC	1	–D	DU	· A	ندن	JJ	
To find CB: As sin. CBD 2	00 E	= '						4		١.	0.400619
Is to sin. CDB			-	•	-	-	•	A	r. C	<i>,</i> 0.	0.409613 9.994916
So is CD	90	40	-	-	-	•	-	-	-	•	2.477121
Buls OD	•		-	-	•	-	•	•	•	-	
To CB 761.47	-		-	-	-	-		-	-	-	2.881650

То	find AB:	,											
	As BC+A	C 12	27.45	-	_	_	-	-	_	Ar	. Co).	6.910995
	Is to BC-	-AC 2	295.4	9 -	-	_	_	_	-	-	-	-	2.470542
	So is tang.	CAB	+CB	A		719	30	ν.			_	1	0.475480
					-	. 1	00				_	_	
	To tang.	CAB-	—CB	A	_	359	44	٤' .			_		9.857017
	To tang.							_				=	
			CE	BA	-	35	46	3					
								_					
	As sin CB			-		-	-	-	-	Ar	. Co	٥.	0.233226
	Is to sin. I			-	-	-	-	-	-	-	-	-	9.779463
	So is CA	465.9	8 -	-,	•	-	-	-	-	-	- •	•	2.668367
	To AB 47	79.8		-	-	-	-	-	-	•	- .		2.681056
		Ev	AMPL]	n 1	Œ	ia	57	Sal	20230	າກຳລາ	-)		
		LIA	AMFL	. T.	(<u>T</u> .	.g.	υι,	Dи	100	yıng	5.)		
To	find C:	_											
		B	3										
		C	2	-	-	-	-	-					698970
	E	BC	1.8	-	-	-	-	-	A	r. (ю.	9.	74472 7
		2	6.8										
	Half su	m	3.4							_		0	531479
	Han su	111						_		_		0.	001110
	Differen	ce	.4	-,		-	-	-	-	-		-1.	602060
											-		
											2):	19.	577236
	Co	s. ½ C	-	59	° 4'	_						9	788618
	00	s. ₂ O					Ū	Ī	Ī	-	=		
		C	-	104	° 8'								
т.	find BD:												
10	As sin. D	170 1	ry i							An	<u> </u>	_	0.515105
	Is to sin. (-	•	•	•	•	AI			9.986651
	So is BC						•					•	0.255273
	20 13 10	110 -				Ī	Ī		Ī		•	-	
	To BD 5.	715 -	-		-	-	-	-	-	-			0.757029

To find CD:
As sin. D Ar. Co 0.515105
Is to sin. DBC 58° 5′ 9.928815
So is BC 0.255273
50 IS DO 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
To CD 5.003 0.699193
Example 5. (Fig. 58, Surveying.)
To find BAC:
A 700
3,020000
AC 8 Ar. Co. 9.096910
27.2
Half sum 13.6 1.133539
Difference 6.4 0.806180
Difference 6.4 0.806180
2)19.957448
Cos. $\frac{1}{2}$ BAC 17° 47' $\frac{1}{2}$ 9.978724
BAC 35° 35
To find AE:
As sin. AEB 136° Ar. Co. 0.158229
Is to sin. EBA 19° 9.512642
So is AB 12 1.079181
·
To AE 5.624 0.750052
To find ACE:
As AC+AE 13.624 Ar. Co. 8.865696
Is to AC—AE 2.376 0.375846
ATIC ACT
So is tang. $\frac{AEC+ACE}{2}$ - 84° 42′ $\frac{1}{2}$ 11.033291
To tang. $\frac{AEC-ACE}{}$ - 62 $1\frac{1}{2}$ 10.274833
To tang. $\frac{1100}{2} - \frac{62}{12} - \frac{11}{2} - \frac{10.274833}{2}$
AEC - 146 44
ACE - 22° 41′
11011 • 22 41

To find AD:						
As sin. ADC 19°					Ar. Co.	0.487358
Is to sin. ACD 22			-			9.586179
So is AC 8			_			0.903090
· To AD 9.476 -						0.976627
To find CD:						
As sin. ADC				-	Ar. Co.	0.487358
Is to sin. DAC 138	° 19′			•		9.822830
So is AC				-		0.903090
		-				
To DC 16.34 -				-		1.213278
To find BD:						
As sin. ADB 44°				-	Ar. Co.	0.158229
Is to sin. BAD 102	° 44′			-		9.989186
So is AB 12 -	- - ,			-		1.079181
To DB 16.85 -						1.226596
Exame	PLE 6.	(Fig.	59, S	urvez	jing.)	
To find ABC:						
AC 4	6					
	0 -	Ar.	Co.		8.301030)
BC 4	.0	Ar.	Co.		8.39794)
0) 10	_					
2)13	66 					
Half sum 6	8 -				1.832509)
Difference 2	_ 0				1.34242)
Difference 2	z - =		•	•	1.042420	,
				2)	19.873902	2
5.				-		-
Cos. ½ ABC	30°	8'		•	9.93695	l
				:		2
ABC	60°	16'				

To find CD and CE:						,	,
As sin. ADC 60° 16′ -	_	_	_	-		Ar. Co.	0.061309
Is to radius	-	-	_	_	_		10.000000
So is AC 46	-	-	-	-	-		1.662758
FR CD							1 501005
To CD 52.98 -	-	-	-	-	-		1.724067
$CE = \frac{1}{2} CD = 26.49$							
AL CAR OO ADC	0.00	,	4 D	a	00	0.44	
Also CAE=90°—ADC=	=90°	— .	AB	U=	29	44.	
Example 7.	(Fi	g. 6	31,	Sur	vej	ying.)	
Making DE radius,		_					nce,
As radius	_	cair Cair	-			Ar. Co.	
Is to tang. D 47° 30' -	-	_	-	-	-	:	10.037948
So is DE 100	-	-	-		-		2.000000
To EC - 109.13 -							0.027049
To EC - 109.13 - EB - 5	-	•	•	-	-		2.037948
17D - 9							
BC - 114.13							
							
Example 8.	(Fi	o. (62.	Sur	rne	uing.)	
To find DC:	(~ .	· o	o. - ,	~ w		9***8*7	
As sin. ACD 25°	_	_	_	_		Ar. Co.	0.374052
Is to sin. CAD 26° 30'			_	_			9.649527
So is AD 75 ft	-	_	_	_ ′	_		1.875061
To DC 79.18 ft	-	-	-	-	-		1.898640
To find BC:							
As radius		_	_	_	_	Ar. Co.	0.000000
Is to sin. CDB 51° 30′	_	_	_	_	_		9.893544
So is CD	-	-			-		1.898640
T. CD clow 6							1.500104
To CB 61.97 ft	-	-	•	-	-		1.792184
Example 9.	(Fi	g. (63,	Sur	rve	ying.)	
To find DC:							
As sin. ACD 23° 50'	-		-		-	Ar. Co.	0.393535
Is to sin. CAD 44° -	-	-	-	-	-		9.841771
So is AD 134	-	-	-	-	-		2.127105
To DC 230.4							2.362411
TO DO 200.7					-	-	2.002411

To find CE:	
As sin. CED 141° Ar. Co.	0.201128
Is to sin. CDE 16° 50'	9.461782
So is CD	2.362411
50 IS OD	
To CE 106	2.025321
To find EB:	
As radius Ar. Co.	0.000000
Is to sin. CDB 67° 50′	9.966653
So is CD	2.362411
To CB 213.3	0.000004
	2.329064
CE 106	
	
BE 107.3	
	•
Example 10. (Fig. 64, Surveying.)	
To find BD:	
As sin. CDB 17° 15′ Ar. Co.	0.527914
Is to sin. BCD 23° 45'	9.605032
So is CB 60	1.778151
20 IS 0B 00	
To BD 81.49	1.911097
To find AD:	
As BD+BA 121.49 Ar. Co.	7.915460
Is to BD—BA 41.49	1.617943
So is tang. BAD+BDA - 69° 30'	10.427262
50 is tailg 00 00	
***	10.421202
To tang BAD BDA 49° 25'	
To tang. BAD BDA - 42° 25'	9.960665
10 fang 42 25	
10 tang 42° 25°	
10 tang 42° 25°	
BDA - 27° 5′	9.960665
BDA - 27° 5′ As sin. ADB 27° 5′ Ar. Co.	9.960665
BDA - 27° 5′ As sin. ADB 27° 5′ Ar. Co. Is to sin. ABD 41°	9.960665 0.341716 9.816943

Example 11. (Fig. 65, Surveying.)

								`	_	- 1		•	, 0			
To	find A	D:														
	As si	n. C.	AD	27	0	-	-	-	-	-	-	-	Ar.	Co.		0.342953
	Is to	sin.	ACI) :	138	3°	-	÷	-	-	-	-	-	•	-	9.825511
	So is	CD	132	2	-	-	-	-	-	-	٠		-		-	2.120574
	To A	D		-	-	-	-	-	-	-	-	-	•	-	-	2.289038
																:
To	find A	В:					-									
	As sin	n. A	BD	10	9°		-	-	-	-	-		Ar.	Co.		0.024330
	Is to	sin.	ADI	B 8	30	-	-	-	-	-	-					9.143555
	So is	AD	-	-	-	-	-	-	-	-	-			-		2.289038
	To A	B 2	8.64	-	-	-	_	-	-	-	-					1.456923

PRACTICAL QUESTIONS.

Example 1. (Pl. 1, fig. 2.)

Making AB radius, BC is tangent of A.

As radius	-	-	-	_		-	-	-	Ar. Co.	0.000000
Is to tang. A	52°	30	,	-	-	-	-	-		10.115020
So is AB 85	-	-	-	٠_		-	-	-		1.929419
To BC 110.8	-	-	-	-	-	-	_	-		2.044439

Example 2. (Pl. 1, fig. 2.)

Make AB radius, then will BC be the tangent of A; making AC radius, AB will be the cosine of A; hence,

- Ar. Co. 0.000000

- - 10.269767

So is AB 73	-	-	-	-	-	-	-	-	-	-	-	-	-	1.863323
To BC 135.9	-	-	-	-	-	-	-	-	-	-	-	-	-	2.133090
And,														
As cosine A	,-	-	-	-	-	-	-	-	-	-	Aı	:. C	0.	0.324845
Is to radius	-	-	-	-		-		-	-	-	-	-	-	10.000000
So is AB -	-	-	-	-	-	-	-	-"	-	-	-	-	-	1.863323
To AC 154.2	-		-	-	-	-	-	-	-	-	-	-	-	2.188168

Example 3. (Pl. 1, fig. 7.)

To find BD. We have in the triangle ABD, the angles and side AB. Hence,

As sin. ADB 31° -							Ar Co	0.988161
Is to sin. BAD 100°	-	-	~	-	-	-		9.993351
So is AB 339	_	-	_	_	-	_		2.530200
To BD 648.2	-	-	-	-	-	-		2.811712

As radius

Is to tang. A 61° 45′ -

Again, in ABC we have the angles, and side AB, to find BC.	Thus,
As sin. ACB 22° 30′ Ar. Co. 0.41716	60
Is to sin. BAC 36° 30′ 9.77438	8
So is AB 339 2.53020	10
To BC 526.9 2.72174	- !8

To BC 526.9	2.721748
In DBC we have the sides DB and BC, and included 72°. To find the side DC. Thus	angle DBC:
$BCD + BDC = 180^{\circ} - 72^{\circ} = 108^{\circ}$.	
Then,	
As BD+BC 1175.1 Ar. Co.	6.929925
Is to BD—BC 121.3	2.083861
So is tang. $\frac{BCD+BDC}{2}$ - 54°	10.138739
To tang. BCD—BDC - 8° 5′	9.152525
BDC 45° 55'	
And,	
As sin. BDC 45° 55′ Ar. Co.	0.143677
Is to sin. DBC 72°	9.978206
So is BC	2.721748
To CD 697.64	2.843631

This example might have been solved by finding AD=496.76,

AC=759.33; whence the angle ADC would be found to be 76° 55', and CD=697.64, as before.

Example 4. (Pl. 1, fig. 8.)

Construction.

With the given distances construct the triangle ABC. Make ACE and CAE respectively equal to 13° 30' and 29° 50'. About the triangle AEC describe the circle ACD. Join EB, and produce it to meet the circumference in D, which will be the situation of the observer.

Since the angles ADE and ACE are subtended by the same arc, we have ADE=ACE=13° 30'. Also CDE=CAE=29° 50'.

0.631815

9.629721

Calculation.

In the triangle ABC, we have the three sides to find the angle BAC. Thus.

	ВС		262										
	A	C	404		Ar.	Co.			7.39	9361	19		
•	Al	В	213		Ar.	Co.			7.67	7162	20		
		2)879										
	Half sum	1	439.5	•		-	-	-	2.6	429	59		
	Difference	ee	177.5	-	•	-	•	-	2.2	491	98		
								2)1	19.9	573	96		
	C	OS. $\frac{1}{2}$	BAC	17°	48'	-	-	-	9.9	786	98		
			BAC	35°	36′								
In th	ne triangle	ACI	E we h	ave tl	he a	ngl	es	anc	l sid	le A	ιC,	to find A	E.
	As sin. AE												
	s to sin.				_		_	_	_			9.368185	
	o is AC				_	_		_		_		2.606381	
Γ	O AE 18	37.43			-	•	-	-	. -	-	-	2.138089	
In	the triang	le A	BE we	e hav	re ti	he :	sid	es	AB	an	d	AE, and	the
includ	ed angle I	BAE:	=BAC	+CA	E=	-65°	2	6′.	T	o fii	nd	ABE, thu	ıs:
A	As AB+A	E . 3	50.43		-	•	-	-	Ar	: C	0.	7.455399	
I	s to AB-				-	-	-	-	••	-	-	1.878349	
S	so is tang.	. <u>A.</u>	$\frac{2B+A}{2}$	BE_	57	° 17	7'	-		•	- :	10.192195	
ŗ	o tang.	AEB	ABI	2	18	° 38	3′	-	-	-	-	9.525943	
			~	BE=	=38	° 44	1'				=		
					=		=						
	ABD·we h												3 0′.
and B	$AD=38^{\circ}$	44'—	-13° 30	' = 25	° 14	1'.	T	o fi	nd .	AD	ar	d DB:	

As sin. ADB 13° 30'

So is AB 213

To BD 389

Is to sin. BAD 25° 14'

And,
As sin. ADB 13° 30′ Ar. Co. 0.631815
Is to sin. ABD 141° 16′ 9.796364
So is AB 213 2.328380
To AD 570.9 2.756559
Finally, in ADC we have the angle ADC=43° 20′, CAD=BAC+BAD=60° 50′ and the side AC; to find CD. Thus,
As sin. ADC 43° 20′ Ar. Co. 0.163523
Is to sin. CAD 60° 50′ 9.941117
So is AC 404 2.606381
To CD 514.1 2.711021
This might have been solved by finding $ACB = 28^{\circ}$ 14′, $CE = 292.87$, whence CBE would have been found to $be = 77^{\circ}$ 26′, $BD = 388.9$, $DC = 514$, and $AD = 570.8$.
Example 5. (Pl. 1, Fig. 9.)
Here $AD = \sqrt{BD^2 - AB^2} = \sqrt{1296} = 36$.
And $AC = AD + DC = 75$ Ans.
Or, Trigonometrically;
As BD 39 Ar. Co. 8.408935
Is to BA 15 1.176091
So is radius 10.000000
To cos. B 67° 23′ 9.585026
And,
As radius Ar. Co. 0.000000
Is to sin. B 67° 23′ 9.965248
So is BD 39 1.591065

1.556313

AC - 75

36

To AD

Example 6. (Pl. 1, fig. 10.)

The angle ACR - DRC - DAC - 25°

The angle $ACD = DDC - DAC = 25$.	
Then,	
As sin ACB 25° Ar. Co.	0.374052
Is to sin. BAC 26° 30′	9.649527
So is AB 75	1.875061
M DC wo to	
To BC 79.18	1.898640
M C I CD I DD	
To find CD, and BD:	
As radius Ar. Co.	0.000000
Is to sin. B 51° 30′	9.893544
So is CB	1.898640
To CD 61.97	1.792184
	===
And,	
As radius Ar. Co.	0.000000
Is to cos. B	9.794150
So is CB	1.898640
· A	
To BD 49.29	1.692790
Example 7. (Pl. 1, fig. 11.)	

Here $ACB = CAD = 35^{\circ}$ and $BAC = 55^{\circ}$

Hence,			-						
As rad		-	-	-	-	-	-	Ar. Co.	0.000000
Is to tan. BA									
So is AB 14	3	-	-	-	-	-	•		2.155336
To BC 204.2	-		-	-	-	-	-		2.310109

Example 8. (Pl. 1, fig. 12.)

Construction.

Make AB=76, the distance from the lower column to the statue's Erect the perpendiculars AD and BF, making the former= With D as a centre and distance 86, cross BF in F, which will be the head of the statue.

Make AI = 64, draw IE parallel to AC, with F as a centre and distance 97, cross IE in E, then EC perpendicular to AC, will be the higher column.

Calculation.

To find FDG and side	ng.				,			
						_	Ar Co	8.065502
Is to FG 76				-				1.880814
		-			-			10.000000
So is radius ·		-	-	•	-	-		10.00000
To sin. FDG 62° 5	1/2 -	-	-	-	-	-		9.946316
As radius		_	_	_	_	_	Ar. Co.	0.000000
Is to cos. FDG 62°	$5\frac{1}{2}'$	-	_		_			9.670300
So is FD 86 -	_	_				_		1.934498
To DG 40.25		-	-	-	-	-		1.604798
To find EFH and FH	I. we	ha	ve	FE	1 = 1	97	and EH	=GI=GI)+
DI=54.25. Hence,	,							0.2 == 0.2 ,
Λs EF 97 ·	_	_	_	_	_	_	Ar. Co.	8.013228
Is to EH 54.25 -		_	_	_	_			1.734400
So is radius			_			_		10.000000
NO IS THUIS								
To sin. EFH 34°-		-	_		٠,			9.747628
And,								
As radius	-	-	-	-	-	•	Ar. Co.	0.000000
ls to cos. F 34° -	-	-	-	-	-	-		9.918574
So is EF 97	_	_		-	-	-		1.986772
To FH 80.42	-	-	٠.	-	-	-		1.905346
						0		
To find ED, we have	re E	:I =	H	\mathbf{F} +	·F(; =	156.42	and DI = 14
Hence,								
As IE 156.42	_		_	_	_	_	Ar. Co.	7.805707
Is to ID 14		-			-	-		1.146128
So is radius	_							10.000000
50 15 Taurus 2 - 2	Ī							
To tan, IED 5° 7'								8.951835
10 talk 11117 0 7		•	•		•	•		

As cos. E 5° 7′ -	-	-	-	-	-	-	-	-	Ar	. Co.	0.001734
Is to rad	-	-	-	-	-	-	-	-	-		10.000000
So is IE 156.42	-	-	-	-	-	-	-	-	-		2.194293
To ED 157.04 -	-	-	-	-	-	-	-	-	-		2.196027

Otherwise.

$$\begin{split} &GD = \sqrt{FD^2 - FG^2} = \sqrt{1620} = 40.25. \\ &GI = GD + DI = 54.25. \\ &FH = \sqrt{FE^2 - EH^2} = \sqrt{6465.9375} = 80.41. \\ &IE = FH + FG = 156.41. \\ &DF = \sqrt{IE^2 + ID^2} = \sqrt{24660.0881} = 157.03. \end{split}$$

SURVEYING.

CHAPTER I.

DIMENSIONS OF A SURVEY.

PROBLEM 8.

EXAMPLE 2.

Angle $B = 34^{\circ} + 35^{\circ} = 69^{\circ}$.

EXAMPLE 3.

Here the first bearing must be reversed, since it is towards the station C. It becomes N. 35° W. Hence $C=180^{\circ}-(35^{\circ}+87^{\circ})=58^{\circ}$.

EXAMPLE 4.

$$D = 180^{\circ} - (87^{\circ} - 58^{\circ}) = 151^{\circ}.$$

PROBLEM 9.

EXAMPLE 2.

1st side S. 40½° E.

N. 54 E.

94½
180

N. 85½ E.

3d N. 29½° E.

N. 54 E.

N. 24¾ W.

24¾ W.

And, As

. ر،٥٠ ،۵٠	DIMENSION	D OF A DO	10 7 12 1 .
4th	N. 28¾° E. N. 54 E.	5t	h N. 57° W. N. 54 E.
	N. 25½ W.		111 180
			S. 69 W.
	6th	S. 47° W. N. 54 E.	
		S. 7 E.	
	E:	KAMPLE 3.	
1 of	S. 45½° W.	2d	N. 50° W.
150	S. $20\frac{1}{2}$ W.	24	S. $20\frac{1}{2}$ W.
	S. 25 W.		N. 70½ W.
3 d	N. 0° W. S. $20^{\frac{1}{2}}$ W.	4th	N. 85° E. S. 20½ W.
	$N. \underbrace{\frac{20\frac{1}{2}}{2}}_{\underline{}} W.$		$N. \overline{64\frac{1}{2}} E.$
5th		7th	
	S. $\frac{50^{\circ}}{67^{\circ}}$ E.		$\frac{3.70^{\frac{1}{2}}}{71^{\frac{3}{4}}}$ W.
			
	PRO	BLEM 10.	
	Ex	AMPLE 1.	
As sin, bea			Ar. Co. 0.269784
	ls		10.000000
So is depa	rture 10.96		1.039811
	e 20.40		1.309595
d,			
			Ar. Co. 0.000000
			10.195813
	rture		
To differen	ce of latitude 17	7.20	1.235624

		Ex	AM	$_{ m PLI}$	E 2	2.				
Λα	distance 44							Α	Co	8.356547
	to difference of la									1.536937
	is radius	inuae	· 0-	r.Tc	,	•	Ī	Ī		10.000000
130	is radius		-	-	-	-	-	-		10.000000
То	cosine of bearing	38° 5	311	_	_	_	_	_		9.893484
	0001110 01 00011115		_							
And,										
•	rad		_	_	_	_	_	Ar	. Co.	0.000000
Is t	to tang. bearing	38° 31	,	_	_	~	_			9.900864
	is diff. lat. 34.43		_	_	_	_	_	_		1.536937
T_0	departure 27.40		_	_	-	_	-	-		1.437801
	•									
		$\mathbf{E}\mathbf{x}$	AM	PL	Е 3					
۸	cosine of bearing							Α		0.072071
					-	-	-			10.000000
	to radius is diff. of lat. 17.2		-	-	-	-	•	-		1.235781
50	is diff. of lat. 17.2	21 -	•	-	-	-	-	-		1.259761
То	distance 20.41		_			_	_	_		1.309752
10	distance 20.41			_						1.000102
And,										
	radius		_	_	_	_	_	Αr	. Co.	0.000000
	tang. bearing 3	2° 30′	_	_	_	_	_	-		9.804187
	is diff. latitude 1			_	_	_	_			1.235781
20	is din. iamudo 1	1.21					•			
To	departure 10.96		_	_	_	_	_	-		1.039968
										====
		Ex	A TAT	PT.I	r 4					
	1100 01 0000			1 1/1		••			~	0.554005
	diff. of lat. 27.92			-	-	-				8.554085
	o departure 5.32		-	-	-	. -	-			***************************************
So :	is radius		-	-	-	-	-	-		10.000000
T _o	tang. bear. 10° 47	, _			_	_				9.279997
10	tang. bear. 10 47	•	-	-	-	-	-	•		=======================================
And,										
	cosine bearing 10	0 47'				_		Δn	Co	0.007737
	o radius	<u> </u>				•				10.000000
	is diff. of lat.		•	•		•	-			1.445915
130 .	is uin. 01 lat.					•	•		•	
То	dist. 28.42			_				-		1.453652

Example 5.

As distance 35.35	-	-	-	-	Ar. Co.	8.451611
Is to departure 15.08 -	-	-	-	-		1.178401
So is radius	-	-	-	-	:	10.000000
•						
To sin. bearing 25° 15'	-	-	-	-		9.630012
			•			
And,						
As radius	-	-	-	-	Ar. Co.	0.000000
Is to cos. bearing 25° 15'	-		-	-		9.956387
So is distance		-	-	-		1.54 8389
To diff. of lat. 31.97 -	-	-	-	-		1.504776

PROBLEM 12.

Sta.	Courses.	Dist.	N.	s.	E.	w.	Cor. N.	Cor. E.	N.	S.	E.	W.
1	N. 75 E.	13.70	3.54		13.24	-	2	2	3.56		13.26	
2	N. 20½ E.	10.30	9.65		3.61		1	1	9.66		3.62	
3	East.	16.20			16.20		2	2	.02		16.22	
4	S. 33½ W.	35.30	,	29.44		19.49	5	5		29.39		19.44
5	S. 76 W.	16.00		3.87		15.52	2	2		3.85		15.50
6	North.	9.00	9.00				1	1	9.01		.01	
7	S. 84 W.	11.60		1.21		11.54	2	2		1.19		11.52
8	N. 53 ¹ ₄ W.	11.60	6.94			9.29	2	2	6.96			9.27
9	N. 363 E.	19.36	15.51		11.59		3	2	15.54		11.61	
10	N. 22½ E.	14.00	12.93		5.36		2	2	12.95		5.38	
11	S. 763 E.	12.00		2.75	11.68		2	2		2.73	11.70	
12	S. 15 W.	10.85		10.48		2.81	2	1		10.46		2.80
13	S. 18 W.	10.62		10.10		3.28	2	1		10.08		3.27
			57.57	57.85	61.68	61.93						
				57.57		61.68						

Error South .28

.25 Error West.

Then

And,

So is diff. lat.

To distance 12.27

0.786041

1.088826

CHAPTER II. SUPPLYING OMISSIONS.

PROBLEM I.

Example 2.

	Sta.	Courses.	Dist.	N.	s.	E.	w.
	1	N. 15¾° W.	9.40	9.05			2.55
	2	N. 63¾ E.	10,43	4.61		9.36	
	3	S. 49 E.	8.12		5.33	6.13	
	4	S. $13\frac{1}{2}$ E.	8.45		8.22	1.98	
	5	S. 163 E.	6.44		6.17	1.86	
	6				(6.11)		(10.64)
	7	N. 60 W.	9.72	4.86			8.41
	8	N. 17 ¹ / ₄ W.	7.65	7.31		2.27	
				25.83	25.83	21.60	21.60
n, A	s d	iff. lat. 6.11 S.				Ar. Co.	9.213959
		depart. 10.64					1.026942
		radius					10.000000
T	o ta	ing. bearing S	. 60° 8′	W			10.240901
1, .	As	cosine bearing	60° 8′		1	Ar. Co.	0.302785
Is	to	radius					10.000000

EXAMPLE 3.

Sta.	Courses.	Dist.	N.	s.	E.	w.
1	S. 52° W.	10.70		6.59		8.43
2	S. $7\frac{1}{2}$ W.	13.92		13.80		1.82
3	S. 34 ¹ / ₄ E.	9.00		7.44	5.07	
4			(27.83)		(5.18)	
				27.83	10.25	10.25

Then,						
				Ar.	Co. 8.55	5487
	s to departure 5.	18				4330
S	o is radius				0.00	0000
T	o tang. bearing	N. 10° 33	8' E		9.26	9817
And,						
	s cosine bearing	10° 33′		Ar.	Co. 0.00	
	to radius				- 10.000	
S	o is diff. lat. 27.8	3			- 1.44	4513
T	o distance 28.31				- 1.45	1917
		Exam	MPLE 4.			
Sta.	Bearing.	Dist.	N.	s.	E.	w.
1	S. 10° E.	92.20		90.80	16.01	
2	S. 15 W.	120.50		116.39		31.19
3	S. $18\frac{1}{2}$ W.	205.00	,	194.40		65.05
4	S. 71½ E.	68.00		21.58	64.49	
5						
				423.17	80.50	96.24 80.50
	·	- ,				15.74
Then,						
A	s diff. of latitude	423.17		Ar.	Co. 7.37	
	s to departure_15	.74				7005
S	o is radius				10.00	0000
Т	o tang. bearing	2° 8′ -			- 8.57	0490
And,						
A	s cosine bearing	2° 8′ -		Ar.	Co. 0.00	
	s to radius	<u> </u>			10.00	
S	o is diff. lat. 423	.17			- 2.62	6515
Т	o distance 423.46	3 - ,			2.62	6816

PROBLEM II.

Example 2.

Sta.	Bearing.	Changed Bearing.	Dist.	N.	S.	E.	w.					
1	S. $40\frac{1}{2}$ E.	N. 85½ E.	31.80	2.49		31.70						
2	N. 54 E.	North.		(2.08)								
3	N. 29½ E.	N. 24 ³ / ₄ W.	2.21	2.01			.93					
4	N. 28¾ E.	N. 25 ¹ / ₄ W.	35.35	31.98			15.08					
5	N. 57 W.	S. 69 W.			(7.49)		(19.51)					
6	S. 47 W.	S. 7 E.	31.30		31.07	3.82						
				38.56	38.56	35.52	35.52					
And	As sine changed bearing 69° Ar. Co. 0.029848 Is to radius 10.000000 So is departure 19.51 1.290257 To distance 5th side 20.90 1.320105 And, As radius Ar. Co. 0.000000 Is to cotang. bearing 69° 9.584177 So is departure 19.51 1.290257											
	To diff. lati	itude 7.49 S				0.874	434					

PROBLEM III.

Example 2.

Sta.	Bearing.	Changed Bearing.	Dist.	N.	S.	. E.	w.
1	S. $40\frac{1}{2}$ E.	N. 85½ E.	31.80	2.49		31.70	
2	N. 54 E.	North.		(2.09)			
3	N. 29½ E.	N. 24¾ W.	2.21	2.01			.93
4	N. E.		35.35	(31.97)			(15.08)
5	N. 57 W.	S. 69 W.	20.90		7.49		19.51
6	S. 47 W.	S. 7 E.	31.30		31.07	3.82	·
				38.56	38.56	35.52	35.52

Then,	
As distance 4th side 35.35 Ar. Co.	8.451611
Is to departure 15.08	1.178401
	10.000000
To sine chang. bearing N. 25° 15′ W 54	9.630012
Bearing 4th side N. 28° 45′ E.	
And,	
As radius Ar. Co.	0.000000
Is to cos. chang. bearing 25° 15'	9.956387
So is distance	1.548389
To diff. latitude 31.97	1.504776
PROBLEM IV.	
TI 0 (D) 1 (10)	

Example 2. (Pl. 1, fig. 13.)

	Bearing.	Dist.	N.	S.	E.	w.
FA	S. E.	31.80				
AB	N. 54 E.	2.08	1.23		1.68	
BC	N. 29½ E.	2.21	1.92		1.08	
CD	N. 283 E.	35.35	31.00		17.00	
DE	N. 57 W.	20.90	11.38			17.52
EF	S. W.	31.30				
Diff.	latitude of	EA	45.53		19.76	17.52
					17.52	ı

Departure of EA 2.24

Then, As diff. lat. EA										8.341702
Is to departure ? So is radius -	2.24	-	-	-	-	-	-	-	-	0.350248
To tang. bearing	EA	2°	49'		-	-	-	-	-	8.691950

And,
As cosine bearing 2° 49′ Ar. Co. 0.000525
Is to radius 10.000000
So is diff. lat 1.658298
To distance EA 45.59 1.658823
To find AEF:
AF 31.80
AE 45.59 Ar. Co. 8.341177
EF 31.30 Ar. Co. 8.504456
2)108.69
Half sum 54.34 1.735120
Difference 22.54 1.352954
2)19.933707
Cos. ½ AEF 22° 6′ 9.966853
AEF 44° 12′
Bearing of EA - 2° 49'
" EF S. 47° 1' W.
To find EAF and bearing of FA:
As AF 31.80 Ar. Co. 8.497573
Is to EF 31.30 1.495544
So is sin. AEF 44° 12′ 9.843336
To sin. EAF - 43° 20' 9.836453
Bearing of EA 2° 49′
" AF 40° 31'

CHAPTER III. CONTENT OF LAND.

PROBLEM I.

EXAMPLE 4.

Here, Area = $176.4 \times 176.4 = 31116.96$ Sq. Perches, = 194 A. 1 R. 36.96 P.

EXAMPLE 5.

Here, Area = $52.25 \times 38.24 = 1998.04$ Sq. Ch. = 199 A. 3 R. 8.64 P.

EXAMPLE 6.

Here, Area = $16.54 \times 12.37 = 204.5998$ Sq. Ch. = 20 A. 1 R. 33.5968 P.

EXAMPLE 7.

Here, Area = $21.16 \times 11.32 = 239.5312$ Sq. Ch. = 23 A. 3 R. 32.4992 P.

PROBLEM 2.

EXAMPLE 2

Here, Area =
$$\frac{18.37 \times 13.44}{2} = \frac{246.8928}{2} = 123.446 \mathfrak{t}$$
 Sq. Ch. = 12 A. 1 R. 15.1424 P.

EXAMPLE 3.

Here, Area =
$$\frac{49 \times 34}{2} = \frac{1666}{2} = 833$$
 Sq. Pe. = 5 A. 0 R. 33 Pe.

PROBLEM 3.

-Example 2. (Pl. 1, fig. 1.)

As radius	 Ar. Co.	0.000000
Is to sin. A 47° 30°	 	9.867631
So is AB \times AC $\left\{ \begin{array}{ll} AB & 15.36 \\ AC & 11.46 \end{array} \right.$	 	1.186391
So is $AB \times AC$ (AC 11.46	 	1.059185
•		
To double area 129.78	 	2.113207

	Committee
Example 3. (Pl. 1, fig. 14.)	
Here, As radius Ar. Co.	0.000000
Is to sin. A 66° 30′	9.962398
(AR 1384	1.141136
So is $AB \times AC$ $\begin{cases} AB & 13.84 & \cdots & \cdots & \cdots \\ AC & 18.23 & \cdots & \cdots & \cdots \end{cases}$	1.260787
	1.200101
To 2 ABC 231.38	2.364321
ABC - $\overline{115.69}$ Ch. = 11 A. 2 R. 11.04 P.	
Example 4. (Pl. 1, fig. 15.)	
Here, As radius Ar. Co.	0.000000
Here, As radius Ar. Co. Is to sin. A 121° 45′	9.929599
~ (AB 19.74	1.295347
	1.239049
To 2 ABC 291.07	2.463995
ABC - 145.535 Ch. = 14 A. 2 R. 8.56 P.	
DDODI DM 4	
PROBLEM 4.	
Example 2. (Pl. 1, fig. 1.)	•
Here, Angle $C = 180$ — $(A + B) = 43^\circ$. Here	nce,
As rad., sin. C \ \frac{\text{radius} Ar. Co.}{\text{Ar. Co.}}	0.000000
(Sin. U 43° - Ar. Uo.	0.166217
Lata sin A sin D (sin. A 63°	9.949881
Is to sin. A, sin. B (sin. B 74°	9.982842
(AB 24.32	1.385964
Is to sin. A, sin. B $\begin{cases} \sin A & 63^{\circ} & - & - & - \\ \sin B & 74^{\circ} & - & - & - \\ \cos AB^{2} & \begin{cases} AB & 24.32 & - & - & - \\ AB & - & - & - & - & - \end{cases}$	1.385964
	2.870868
ABC - 371.4 Ch. = 37 A. 0 R. 22.4 P.	
Example 3.	
Here, the angle $C = 94^{\circ}$ 15'. Hence	
As rad., sin. C { rad Ar. Co. sin. C 94° 15′ Ar. Co. Is to sin. A sin. B { sin. A 37° 30′	0.000000
l sin. C 94° 15' Ar. Co.	0.001196
Is to sin. A, sin. B \(\sin. A \) 37° 30'	9.784447
s to sin. A, sin. B (sin. B 48° 15'	
So : AP2 (AB 17.36	1.239550
So is AB^2 $ \begin{cases} AB & 17.30 \\ AB & \end{cases} $	1.239550
To 2 ABC 137.25	2.137515
ABC -68.625 Ch. = 6 A. 3 R. 18 P.	

PROBLEM 5.

EXAMPLE 2.

Here, 1	0.64 + 12.28 + 9.00 = 31.92 = sum of sides.														
Half sum	15.96 log. 1.203033														
	(5.32 0.725912														
Remainders	3.68 0.565848														
	$ \begin{cases} 5.32 & - & - & - & - & 0.725912 \\ 3.68 & - & - & - & - & 0.565848 \\ 6.96 & - & - & - & - & - & 0.842609 \end{cases} $														
	2)3.337402														
Area	10)46.63 Ch 1.668701														
	4.000 4.4 0.D 00.00 D														
	4.663 = 4 A. 2 R. 26.08 P.														
	Example 3.														
	re, $20+30+40 = 90 = \text{sum of sides}$.														
Half sum	45 1.653213														
	(25 1.397940														
Remainders	$\begin{cases} 25 & - & - & - & - & - & - & 1.397940 \\ 15 & - & - & - & - & - & - & 1.176091 \\ 5 & - & - & - & - & - & - & 0.698970 \end{cases}$														
	(5 0.698970														
	2)4.926214														
	10)290.47 2.463107														
	29.047 A. = 29 A. 0 R. 7.52 P.														
PROBLEM 6.															
	Example 2.														

Here,
$$16.10 \times \frac{6.80 + 3.40}{2} = 16.1 \times 5.1 = 82.11 \text{ Ch.}$$

= 8 A. 0 R. 33.76 P.

Example 3.

Here,
$$24 \times \frac{8.27 + 12.43}{2} = 24 \times 10.35 = 248.4$$
 Ch. $= 24$ A. 3 R. 14.4 P.

PROBLEM 7.

EXAMPLE 2.

Here, Area =
$$\frac{12.41 + 8.22}{2} \times 5.15 = 53.12225$$
 Ch. = 5 A. 1 R. 9.956 P.

Example 3.

Here, Area =
$$\frac{11.34 + 18.46}{2} \times 13.25 = 197.425$$
 Ch. = 19 A. 2 R. 38.8 P

PROBLEM 9.

EXAMPLE 2.

S. Areas.	•		104.2568	32.1440		7.2653	143.6661 48.7660
N. Areas.	15.3660	7.2600			26.0400		48.7660
D. M. D.	2.60	4.00	14.44	16.40	10.85	7.49	
W.	2.60			4.48	1.07	2.29	10.44
pi .		4.00	6.44	-			10.15 10.44
αį			7.22	1.96		76.	
z	5.91	1.84			2.40		10.15
Cor. S. Cor. W.	0	0	F	0	O	0	-
Cor. S.	0	0	1	0	0	0	Н
W.	2.60			4.48	1.07	2.29	10.44
ĕ	,	4.00	6.45				10.45
αį			7.21	1.96		.97	10.14
ż	5.91	1.84			2.40		$\frac{10.15}{10.14}$
Dist.	6.46	4.40	9.68	4.895	2.625	2.49	30.550
Bearing.	N. 28° 45′ W.	N. 65° 16′ E.	S. 41° 49′ E.	S. 66° 22′ W.	N. 24° 2′ W.	S. 66° 59′ W.	
Sta.	-	62	တ	4	5	9	

Area, 4 A. 2 R. 39.2 P.

47.4500 2)94.9001

.01 Error W.

Error S. .01

4.745

2.53812 40

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---|
| S. Areas. | 87.1194 | | | | | | | 105.8068 | , 104,4415

 |
 | | | 341.6366 | 408.6259
 | 275.6880 | 254.8931 | | | | | | | |
 | 1578.2113
685.5207 | 2)892.6906 | 446.3453 |
| N. Areas. | | 59.4594 | 57.0757 | 36.0393 | 11.4632 | 36.8904 | 33,3639 | |

 | .3381
 | 223.0249 | 49.6800 | |
 | | | 178.1858
 | 685,5207 | | |
| D. M. D. | 24.61 | 13.86 | 9.79 | 4.89 | 3.56 | 8.09 | 13.73 | 19.03 | 23.47

 | 33.81
 | 40.33 | 43.20 | 50.02 | 50.51
 | 50.40 | 47.29 | 36.07
 | | | 25 P. |
| W. | 69.9 | 4.06 | 10. | 4.89 | | | | |

 |
 | 10. | | | 3.45
 | | 6.45 | 4.77
 | | | 21.5 |
| <u>면</u> | - | | | | 3.56 | .97 | 4.67 | .63 | 3.81

 | 5.53
 | | 2.88 | 3.94 | | | | | | |
 | 3.34 | |
 | | | 2 R. |
| ν <u>ά</u> | 3.54 | i | | | | | | 92.0 |

 |
 | <u></u> | | | 3.09
 | | 9.36 |
 | | | 44 A. |
| _ | | 20 | 83. | .37 | .22 | .56 | .43 | 4.5 | 4

 | 0.
 | .53 | .15 | | ω
 | 44.0 | 4.5 | .94
 | | | Area, 44 A. 2 R. 21.525 P. |
| | | 1 | 1 | 1 | 1 | 4 | CX | |

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 | | | ₹. |
| Cor. 1 | _ | - | - | - | - | 0 | - | - | -

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 | - | 0 | - | -
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 | | | |
| Cor. N. | 1 | 1 | - | 1 | 0 | 0 | 0 | 1 | 1

 | 1
 | F -1 | 0 | 1 | 1
 | 1 | 1, | 1
 | | 闰 | |
| W. | 6.68 | 4.05 | | 4.88 | | | | |

 |
 | | | | 3.44
 | | 6.44 | 4.76
 | 30.25 | Error | |
| Ξ. | | | | | 3.57 | 76. | 4.68 | .64 | 3.85

 | 6.54
 | | 2.88 | 3.95 |
 | 3.35 | |
 | 30.40 | 15 | |
| σż | 3.55 | | <u> </u> | | | | | 5.57 | 4.46

 |
 | | | 6.84 | 8.10
 | 5.48 | 5.40 | | | | | | | |
 | 9.41 | 122 | |
| N. | | 4.28 | 5.85 | 7.36 | 3.22 | 4.56 | 2.43 | |

 |
 | 5.52 | 1.15 | |
 | | | 4.93
 | 9.27 | 'n | |
| Dist. | 7.57 | <u> </u> | <u> </u> | <u> </u> | <u> </u> | | | 9.60 | 2.87

 | 3.54
 | 1 | 3.10 | 7.90 | 8.80
 | 3.42 | 3.40 |
 | <u> </u> | Erro | |
| Bearing. | S. 62° W. | N. 43½ W. | North. | N. 33½ W. | N. 48 E. 4 | N. 12 E. 4 | N. 62½ E. | S. 6½ E. | S. 40½ E.

 | East.
 | North. | N. 684 E. | |
 | S. 31½ E. (| S. 50 W. | N. 44 W.
 | | | |
| Bta. | - | 2 | က | 4 | 10 | 9 | 1 | 000 | 6

 | 10
 | 11 | 12 | 13 | 14
 | 15. | 91 | 17
 | | | |
| | Bearing. Dist. N. S. E. W. Cor. W. Cor. W. N. S. E. W. D. M. D. N. D. N. Areas. | Bearing. Dist. N. S. E. W. Cor. N. Cor. W N. S. E. W. D. M. D. M. D. N. Areas. S. 620 W. 7.57 3.55 6.68 1 1 3.54 6.69 24.61 | Bearing. Dist. N. S. E. W. Cor. N. Cor. N. Cor. W. N. S. E. W. D. M. D. N. Areas. S. S. 62° W. 7.57 3.55 6.68 1 1 3.54 6.69 24.61 N. Areas. 8 N. 43½ W. 5.89 4.28 4.05 1 1 4.06 13.86 59.4594 | Bearing. Dist. N. S. E. W. Cor. W. N. Cor. W. N. S. E. W. D. N. D. N. Areas. F. S. 62° W. 7.57 3.55 6.68 1 1 4.29 6.69 24.61 59.4594 6.94594 N. 43½ W. 5.82 5.82 1 1 4.29 4.06 13.86 59.4594 6.69 North. 5.82 5.82 1 1 1 5.83 .01 9.79 57.0757 | Bearing. Dist. N. S. E. W. Cor. W. N. S. F. W. D. M. D. N. Areas. F. S. 62º W. 7.57 3.55 6.68 1 1 4.29 24.61 5.4 | Bearing. Si. Br. N. 5. | Bearing. Dis. N. S. E. W. Cor. N. N. S. F. W. D. N. D. N. Areas. F. S. 62° W. 7.57 3.55 6.68 1 1 4.29 0.0 | Bearing. Dis. N. S. E. W. Cor. W. N. S. E. W. D. N. D. N. Areas. F. S. 62° W. 7.57 3.55 6.68 1 1 4.29 8.69 24.61 N. Areas. F. N. 43½ W. 5.89 4.28 1 1 4.29 4.06 13.86 59.4594 7. N. 43½ W. 5.82 5.82 1 1 1 5.83 4.06 9.79 57.0757 7. N. 48 E. 4.81 3.22 3.57 0 1 3.22 3.56 11.4632 7. N. 12 E. 4.66 4.56 9 0 4.56 9 8.09 86.8904 8. N. 62½ E. 5.77 2.43 4.68 0 1 2.43 4.67 13.73 33.3639 | Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. Or. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 4.06 24.61 6.69 24.61 6.69 24.51 7.34 6.69 24.61 6.69 24.61 6.69 24.61 6.63 1 1 2.83 7.96 13.86 6.945.94 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.61 6.69 24.69 6.79 4.89 6.70 6.70 6.79 4.89 11.4632 8.69 11.4632 8.69 11.4632 8.69 8.69 8.69 <t< td=""><td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. N. Areas. N. 43½ W. 5.89 4.28 1 1 5.83 7.06 13.86 59.4594 N. Areas. N. 43½ W. 5.83 7.36 1 1 7.37 1 4.89 36.0393 N. Areas. N. 43½ W. 5.83 7.36 1 1 7.37 1 4.89 36.0393 N. Areas. N. 43½ W. 8.83 7.36 3.57 0 1 3.22 3.56 3.56 11.4632 N. Areas. N. 45½ E. 4.66 4.66 0 0 4.56 .97 8.09 8.6894 N. Areas. S. 6½ E. 5.57 2.43 4.67 1 13.73<!--</td--><td>Bearing. Dist. N. S. E. W. Cor. W. N. S. E. W. Cor. N. Cor. N. N. S. E. W. D. M. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 D. M. D. N. Areas. N. 43½ W. 5.89 4.28 1 1 5.83 .01 97.9 57.4594 2.46 N. 43½ W. 5.83 7.36 1 1 7.37 2 4.89 36.0393 36.0393 N. 43½ W. 8.83 7.36 3.57 0 1 3.22 3.56 3.56 11.4632 36.0393 N. 43 E. 4.66 4.66 0 0 4.56 .97 8.09 36.8904 8.09 N. 45 E. 5.70 2.43 4.67 3.74 8.09 36.8904 9.0 N. 62½ E. 5.77 2.43 4.67 3.91 33.3639 9.0</td><td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. 8.69 24.61 N. Areas. N. 43½ W. 5.89 4.28 1 1 5.83 0 13.86 57.0757 14.89 14.89 57.0757 14.89</td><td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. A. E. W. D. N. D. N. Areas. P. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. P. Areas</td><td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.54 6.68 1 1 4.29 24.61 N. Areas. N. Areas. N. 43½ W. 5.89 4.28 1 1 4.29 3.66 13.86 59.4594 N. Areas. N. 43½ W. 5.82 5.82 1 1 1 4.89 4.89 59.4594 N. Areas. N. 33½ W. 8.83 7.36 4.88 1 1 7.37 4.89 4.89 56.0393 N. Areas. N. 33½ W. 8.83 7.36 4.88 1 1 7.37 4.89 4.89 36.0393 N. Areas. N. 63½ E. 4.66 9 1 2.43 4.67 1.37.3 8.09 8.09 8.09 8.09 8.09 9.00 1.97 8.46 1.90<!--</td--><td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. 8.94594 N. Areas. N. 43½ W. 5.82 4.26 1 1 1 4.89 4.06 13.86 59.4594 N. Areas. N. 3½ W. 5.82 7.36 4.88 1 1 7.37 4.89 4.89 56.0393 N. Areas. N. 3½ W. 5.83 7.36 1 1 7.37 4.89 4.89 56.0393 N. Areas. N. 3½ W. 5.83 4.66 0 1 2.45 4.89 36.0393 N. Areas. N. 6½ E. 5.67 4.66 0 0 4.56 9.97 19.03 8.89 14.68 14.69 14.69 11.4632 14.69 11.60</td><td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. D. M. D. N. Areass. S. 62° W. 7.57 3.55 6.68 1 1 4.29 N. 4.06 1.86 1 4.29 N. 4.06 1.86 1 1.85 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 4.06 1.01 9.79 4.06 1.04 9.79 4.06 1.04 9.79 4.89 59.4594 N. 4.89 1.04 9.79 4.89 36.0393 N. 4.89 1.04 9.79 4.89 36.0393 N. 4.89 4.89 36.0393 N. 4.89 4.8</td><td>S. 62° W. N. A. S. E. W. Cor. W. Cor. W. N. A. S. E. W. D. M. D. N. Areas. S. 62° W. 7.57 3.54 6.68 1 1 4.29 4.06 13.86 59.4594 8.0.0 N. 43½ W. 5.89 4.28 1 1 5.83 1.01 9.79 57.0757 9.79 57.0757 N. 43½ W. 5.83 7.36 4.88 1 1 7.37 4.89 4.89 56.04594 9.70 <t< td=""><td>S. 62° W. Dist. N. S. E. W. Cor. W. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.59 4.28 1 1 4.29 4.06 24.61 N. Areas. N. 43½ W. 5.89 4.28 4.65 1 1 4.29 4.06 13.86 55.4594 8.09 N. 48 E. 4.81 3.22 4.88 1 1 7.37 4.89 4.89 56.0393 N. 48 E. 4.81 3.22 3.57 0 1 3.22 3.56 4.89 36.0393 N. 48 E. 4.81 3.22 3.57 4.68 0 1 3.23 4.89 36.0393 N. 62½ E. 5.27 2.43 4.68 0 1 2.43 4.67 11.4632 S. 40½ E. 5.67 4.46 3.82 1 1 4.45 3.81 1.37 S. 30 E. 5.57 4.49<</td><td>S. 62° W. 7.57 3.5 E. W. Cor. W. W. S. F. W. D. M. D. N. Areas. N. 43½ W. 589 4.25 4.05 1 1 4.29 4.06 24.61 0.0. N. <t< td=""><td>S. 62° W. N. 54 N. 65 N. 757 N. 758 N. 757 N. 757 N. 758 N. 757 N. 757 N. 758 N. 757 N. 758 N. 758</td></t<></td></t<></td></td></td></t<> | Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. N. Areas. N. 43½ W. 5.89 4.28 1 1 5.83 7.06 13.86 59.4594 N. Areas. N. 43½ W. 5.83 7.36 1 1 7.37 1 4.89 36.0393 N. Areas. N. 43½ W. 5.83 7.36 1 1 7.37 1 4.89 36.0393 N. Areas. N. 43½ W. 8.83 7.36 3.57 0 1 3.22 3.56 3.56 11.4632 N. Areas. N. 45½ E. 4.66 4.66 0 0 4.56 .97 8.09 8.6894 N. Areas. S. 6½ E. 5.57 2.43 4.67 1 13.73 </td <td>Bearing. Dist. N. S. E. W. Cor. W. N. S. E. W. Cor. N. Cor. N. N. S. E. W. D. M. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 D. M. D. N. Areas. N. 43½ W. 5.89 4.28 1 1 5.83 .01 97.9 57.4594 2.46 N. 43½ W. 5.83 7.36 1 1 7.37 2 4.89 36.0393 36.0393 N. 43½ W. 8.83 7.36 3.57 0 1 3.22 3.56 3.56 11.4632 36.0393 N. 43 E. 4.66 4.66 0 0 4.56 .97 8.09 36.8904 8.09 N. 45 E. 5.70 2.43 4.67 3.74 8.09 36.8904 9.0 N. 62½ E. 5.77 2.43 4.67 3.91 33.3639 9.0</td> <td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. 8.69 24.61 N. Areas. N. 43½ W. 5.89 4.28 1 1 5.83 0 13.86 57.0757 14.89 14.89 57.0757 14.89</td> <td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. A. E. W. D. N. D. N. Areas. P. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. P. Areas</td> <td>Bearing. Dist. N. 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N. 33½ W. 8.83 7.36 4.88 1 1 7.37 4.89 4.89 56.0393 N. Areas. N. 33½ W. 8.83 7.36 4.88 1 1 7.37 4.89 4.89 36.0393 N. Areas. N. 63½ E. 4.66 9 1 2.43 4.67 1.37.3 8.09 8.09 8.09 8.09 8.09 9.00 1.97 8.46 1.90 </td <td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. 8.94594 N. Areas. N. 43½ W. 5.82 4.26 1 1 1 4.89 4.06 13.86 59.4594 N. Areas. N. 3½ W. 5.82 7.36 4.88 1 1 7.37 4.89 4.89 56.0393 N. Areas. N. 3½ W. 5.83 7.36 1 1 7.37 4.89 4.89 56.0393 N. Areas. N. 3½ W. 5.83 4.66 0 1 2.45 4.89 36.0393 N. Areas. N. 6½ E. 5.67 4.66 0 0 4.56 9.97 19.03 8.89 14.68 14.69 14.69 11.4632 14.69 11.60</td> <td>Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. D. M. D. N. Areass. S. 62° W. 7.57 3.55 6.68 1 1 4.29 N. 4.06 1.86 1 4.29 N. 4.06 1.86 1 1.85 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 4.06 1.01 9.79 4.06 1.04 9.79 4.06 1.04 9.79 4.89 59.4594 N. 4.89 1.04 9.79 4.89 36.0393 N. 4.89 1.04 9.79 4.89 36.0393 N. 4.89 4.89 36.0393 N. 4.89 4.8</td> <td>S. 62° W. N. A. S. E. W. Cor. W. Cor. W. N. A. S. E. W. D. M. D. N. Areas. S. 62° W. 7.57 3.54 6.68 1 1 4.29 4.06 13.86 59.4594 8.0.0 N. 43½ W. 5.89 4.28 1 1 5.83 1.01 9.79 57.0757 9.79 57.0757 N. 43½ W. 5.83 7.36 4.88 1 1 7.37 4.89 4.89 56.04594 9.70 <t< td=""><td>S. 62° W. Dist. N. S. E. W. Cor. W. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.59 4.28 1 1 4.29 4.06 24.61 N. Areas. N. 43½ W. 5.89 4.28 4.65 1 1 4.29 4.06 13.86 55.4594 8.09 N. 48 E. 4.81 3.22 4.88 1 1 7.37 4.89 4.89 56.0393 N. 48 E. 4.81 3.22 3.57 0 1 3.22 3.56 4.89 36.0393 N. 48 E. 4.81 3.22 3.57 4.68 0 1 3.23 4.89 36.0393 N. 62½ E. 5.27 2.43 4.68 0 1 2.43 4.67 11.4632 S. 40½ E. 5.67 4.46 3.82 1 1 4.45 3.81 1.37 S. 30 E. 5.57 4.49<</td><td>S. 62° W. 7.57 3.5 E. W. Cor. W. W. S. F. W. D. M. D. N. Areas. N. 43½ W. 589 4.25 4.05 1 1 4.29 4.06 24.61 0.0. N. <t< td=""><td>S. 62° W. N. 54 N. 65 N. 757 N. 758 N. 757 N. 757 N. 758 N. 757 N. 757 N. 758 N. 757 N. 758 N. 758</td></t<></td></t<></td> | Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. Cor. N. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.55 6.68 1 1 4.29 24.61 N. Areas. 8.94594 N. Areas. N. 43½ W. 5.82 4.26 1 1 1 4.89 4.06 13.86 59.4594 N. Areas. N. 3½ W. 5.82 7.36 4.88 1 1 7.37 4.89 4.89 56.0393 N. Areas. N. 3½ W. 5.83 7.36 1 1 7.37 4.89 4.89 56.0393 N. Areas. N. 3½ W. 5.83 4.66 0 1 2.45 4.89 36.0393 N. Areas. N. 6½ E. 5.67 4.66 0 0 4.56 9.97 19.03 8.89 14.68 14.69 14.69 11.4632 14.69 11.60 | Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. D. M. D. N. Areass. S. 62° W. 7.57 3.55 6.68 1 1 4.29 N. 4.06 1.86 1 4.29 N. 4.06 1.86 1 1.85 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 59.4594 N. 4.06 1.82 4.06 1.01 9.79 4.06 1.04 9.79 4.06 1.04 9.79 4.89 59.4594 N. 4.89 1.04 9.79 4.89 36.0393 N. 4.89 1.04 9.79 4.89 36.0393 N. 4.89 4.89 36.0393 N. 4.89 4.8 | S. 62° W. N. A. S. E. W. Cor. W. Cor. W. N. A. S. E. W. D. M. D. N. Areas. S. 62° W. 7.57 3.54 6.68 1 1 4.29 4.06 13.86 59.4594 8.0.0 N. 43½ W. 5.89 4.28 1 1 5.83 1.01 9.79 57.0757 9.79 57.0757 N. 43½ W. 5.83 7.36 4.88 1 1 7.37 4.89 4.89 56.04594 9.70 <t< td=""><td>S. 62° W. Dist. N. S. E. W. Cor. W. N. S. E. W. D. N. D. N. Areas. S. 62° W. 7.57 3.59 4.28 1 1 4.29 4.06 24.61 N. Areas. 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B. 9	٠,]				O N	тЕ	NT	0 1	LA	ND	•			39
	S. Areas.	140.8512	3139.4082	1024.3012				274.8888	4579.4494 936.7313	2)3642.7181	1821.35905	182.135905	.543620	21.744800
	N. Areas.				504.3913	129.8400	302.5000		936.7313					
	D. M. D.	73.36	106.71	91.13	38.71	0.00	22.00	47.07						
	W.			(25.71)	26.71	00.9	-		58.42					
	펵	23.22	10.13				22.00	3.07	58.42					
	oğ.	1.92	29.42	(11.24)				5.84	48.42			•		
	Ä.				13.03	21.64	13.75		48.42					
	Dist.	23.30	31.12		29.72	22.46	25.94	09.9						
	Bearing.	S. 85\frac{1}{4} E.	. S. 19 E.		N. 64 W.	N. $15\frac{1}{2}$ W.	N. 58 E.	S. 273 E.						
	Sta.	1	2	က	4	5	9	7						
Is So	to is	depa radi		e 2	5.71 - 66°	23′	-			- - -	r. Co - -	- 1.43 - 10.00	49234 10102 00000 59336	
Is So	to is	radi diff.		11.2		23'	-			A1	·. Co	- 10.00 - 1.05	97272 90000 50766 48038	

2.57562023,02480

81.643905

Ехамиль 5. (Р. 2, fig. 4.)

S. Areas.	128.4228				256.6014	1498.6174	323.2198		2206.8614 573.9833	2)1632.8781	816.43905
N. Areas.		129,9802	122.8304	247.4502				73.7225	573.9833		
D. M. D.	25.38	8.18	12.32	26.02	45.74	70.49	61.10	39.85			
W.	9.05	8.18					15.80	5.45			
E.			12.32	1.38	18.34	6.41					
vi	5.06				5.61	21.26	5.29				
N.		15.89	9.97	9.51				1.85			
Cor.						-					
Cor.						1					
W.	9.05	8.18					15.80	5.45	38.45		
떠			12.32	(1.38)	(18.34)	6.40			38.44 38.45		
vá	5.06				(5.61)	21.27	5.29		37.23		
Ŋ.		15.89	9.97	(9.51)				1.85	.23		
Dist.	10.34	17.88	15.85	19.61	19.18	22.21	16.65	5.76			
Bearing.	S. 603 W.	N. 274 W.	N. 51 E.	N. $(8\frac{1}{4})$ E.	S. (73°) E.	S. 163 E.	S. 71½ W.	N. 714 W.			
Sta.	1	cs	က	4	ပ	9	7	œ			

Area 81 A. 2 R. 23,0248 P.

As diff. lat. DF 3.91 Ar. Co. 9.407823 Is to depart. 19.73 1.295127 So is radius 0.000000
To tang. bearing N. 78° 47′ E 10.702950
As cosine bearing 78° 47′ Ar. Co. 0.711036 Is to radius 10.000000 So is diff. latitude 3.91 0.592177
To distance DF 20.10 1.303213
FE 19.18 ED 9.61 Ar. Co. 9.017277 DF 20.10 " " 8.696804 2)48.89
Half sum 24.445 1.388190
Diff. 5.265 0.721398
2)19.823669
Cos. $\frac{1}{2}$ FDE 35° 17' 9.911834
FDE 70° 34′ Bearing DF N. 78 47 E.
Bearing DE N. 8° 13' E.
As FE 19.18 8.717151 Is to DE 9.61 0.982723 So is sin. FDE 70° 34′ 9.974525
To sin. DFE* 28° 12' 9.674399
Bearing FD S. 78 47 W.
106 59 180
Bearing EF S: 73 1 E.

Area 244 A. 3 R. 4.9632 P.

Example 6. (Fig. 81, Surveying.)

S. Areas.					191.6096		2260,3448	2513,7531		2205.2862	393,3658	7564.3595	2)4895.6204 2447.8102 244.78102 4
N. Areas.	797.2764	26.8068	10.6032	184.5135		1519.9920			129.5472			2668,7391	
D. M. D.	30.12	15.06	.48	15.65	52.64	83.70	109.09	117.63	94.56	77.46	52.73		
W.		15.06						8.09	14.98	2.12	(22.61)	62.86	
ធ			.48	14.69	22.30	8.76	16.63					62.86	
zi.					3.64		20.72	21.37		28.47	(7.46)	81.66	
ż	(26.47)	1.78	22.09	11.79		18.16			1.37			81.66	
Dist.		15.16	22.10	18.83	22.60	20.17	26.57	22.86	15.04	28.55			
Changed bearing.	North.	N. 834 W.	N. 14 E.	N. 514 E.	S. 803 E.	N. 25\frac{3}{4} E.	S. 38\frac{3}{4} E.	S. $20\frac{3}{4}$ W.	N. 84\frac{3}{4} W.	S. 44 W.	S. 713 W.		
Bearing.	N. 514 W.	S. 45½ W.	N. 50 W.	North.	N. 48 E.	N. 25½ W.	East.	S. 30½ E.	Ś. 44 W.	S. 47 E.	S. 20½ W.		
. Sta.	AB	BC	CD	DE	EF	FG	В	HI	IK	KL	LA		

	As sine changed										
	Is to radius -										
	So is departure	22.61	-	-	-	-	-	-	-		1.354301
											
	To distance LA	23.83	l	-	-	-	-	-	-		1.376715
And	l ,										
	As radius		-	-	-	-	-	-	-	Ar. Co.	0.000000
	Is to cotang. be	aring	-	-	-	-	-	-	-		9.518184
	So is departure		-	-	-	-	-	-	-		1.354301
	To diff. latitude	7.46	-	-	-	-	-	-	-		0.872485

Example 7. (Fig. 80, Surveying.) To find the third side.

Sta.	Bearing.	Dist.	N.	S.	E.	w.
EA	S. 52 W.	10.70		6.59		8.43
AB	S. 7½ W.	13.92		13.80		1.82
BC	S. 33½ E.	9.00		7.53	4.93	
				27.92	ļ	$ \begin{array}{r} 10.25 \\ 4.93 \\ \hline 5.32 \end{array} $

As diff. lat. EC 27.92 -	-	-	-	100	-	-	Ar	. C	0.	8.554085
Is to depart. 5.32	-	-	-	-	-	1	-	-	-	0.725912
So is radius	-	-	-	-	-	-	-	-	-	10.000000
To tang. bearing S. 10°	47′	W	•	-	-	-	-	-	-	9.279997
As cosine bearing 10° 4'	7,	_					Δ 10	C	^	0.007737
As cosine bearing to 4	•		-			_	21.1	. 0	υ.	0.001101
Is to radius	-	-	-	-	-	-	-	-	-	10.000000
So-is diff. lat	-	-	-	-	-	-	-	-	-	1.445915
To distance 28.42	-	-	-	=	-	-	-	-	-	1.453652

8ta. Bearing. Dist. N. S. E. W. Cor. N. N. S. E. W. D. M. D. N. Areas. S. Areas. 1 North. 7.81 7.81 7.81 4.32 17.63 3 3 4.35 17.60 50.68 257.7711 220.4580 2 S. 10\frac{3}{4} W. 2842 27.92 27.92 5 4 27.97 5.35 62.93 17.60 17.60 50.68 17.60.1521 1760.1521 4 N. 844 W. 27.12 2.72 26.98 5 4 2.67 27.92 30.56 81.5952 1760.1521 5 N. 44 W. 22.00 21.93 1.73 4 4 2.189 1.77 1.77 38.7453 16.55 6 East. 16.58 3 3 3 16.55 16.55 16.55 16.55 16.55 16.55 16.55 16.55 16.55 16.55 16.55 16.55 16.55 16.55								
Bearing. Dist. N. S. E. W. Cor. S. Cor. W. N. S. E. W. D. M. D. N. S. E. W. D. M. D. N. D. M. D. N. N. N. S. I. T.779 N. S. I. N. I. I.<	S. Areas.		220.4580	1760.1521			.4965	1981.1066 378.1116
Bearing. Dist. N. S. E. W. Cor. S. Cor. W. N. S. E. W. North. 7.51 7.73 4.32 17.63 2 1 7.79 9 01 S. 10\frac{3}{4} W. 28.42 27.92 27.92 5.30 5 4 27.97 5.35 N. 84\frac{4}{4} W. 27.12 2.72 26.98 5 4 2.67 27.02 N. 4\frac{1}{4} W. 22.00 21.93 1.73 4 4 21.89 1.77 East. 16.58 3 3 3 16.55 1 120.08 32.46 32.24 34.21 34.01 3 3 16.55 1	N. Areas.	257.7711			81.5952	38.7453		378.1116
Bearing. Dist. N. S. E. W. Cor. S. Cor. W. N. S. E. North. 7.81 7.81 4.32 17.63 3 3 4.35 17.60 S. 10\frac{3}{4} W. 28.42 27.92 27.92 5.30 5 5 57.97 7.79 N. 84\frac{1}{4} W. 27.12 2.72 26.98 5 4 26.7 2 2 N. 4\frac{1}{4} W. 22.00 21.93 1.73 4 4 21.89 2 2 East. 16.58 3 3 3 .08 16.55	D. M. D.	33.09	50.68	62.93	30.56	1.77	16.55	
Bearing. Dist. N. S. E. W. Cor. S. Cor. W. N. S North. 7.81 7.81 2 1 7.79 S. 764 E. 18.15 4.32 17.63 3 3 4 S. 103 W. 28.42 27.92 5.30 5 5 5 77 N. 844 W. 27.12 2.72 26.98 5 4 2.67 7 N. 4½ W. 22.00 21.93 16.58 3 3 3 3 East. 16.58 32.24 34.21 34.21 34.01 3 3	W.	10.		5.35	27.02	1.77		
Bearing. Dist. N. S. E. W. Cor. S. Cor. W. N. S North. 7.81 7.81 2 1 7.79 S. 764 E. 18.15 4.32 17.63 3 3 4 S. 103 W. 28.42 27.92 5.30 5 5 5 77 N. 844 W. 27.12 2.72 26.98 5 4 2.67 7 N. 4½ W. 22.00 21.93 16.58 3 3 3 3 East. 16.58 32.24 34.21 34.21 34.01 3 3	ë		17.60				16.55	
Bearing. Dist. N. S. E. W. Cor. S. Cor. W. North. 7.81 4.32 17.63 2 1 S. 764 E. 18.15 4.32 17.63 3 3 S. 103 W. 28.42 27.92 55.30 5 4 N. 844 W. 27.12 2.72 26.98 5 4 N. 4½ W. 22.00 21.93 1.73 4 4 2 East. 16.58 32.24 34.21 34.01 3 3 3	ιά		4.35	27.97			.03	
Bearing. Dist. N. S. E. W. North. 7.81 7.81 4.32 17.63 . S. 103/4 W. 28.42 27.92 5.36 N. 844/4 W. 27.12 2.72 26.93 N. 4½/4 W. 22.00 21.93 1.75 East. 16.58 16.58 1.75 East. 16.008 32.46 32.24 34.21 34.01	l	7.79			2.67	21.89		
Bearing. Dist. N. S. E. W. North. 7.81 7.81 4.32 17.63 . S. 103/4 W. 28.42 27.92 5.36 N. 844/4 W. 27.12 2.72 26.93 N. 4½/4 W. 22.00 21.93 1.75 East. 16.58 16.58 1.75 East. 16.008 32.46 32.24 34.21 34.01	Cor.W.	-	ಣ	5	4	4	က	
Bearing. Dist. N. S. E. W. North. 7.81 7.81 4.32 17.63 . S. 10\frac{3}{4} W. 28.42 27.92 27.92 5.36 N. 84\frac{1}{4} W. 27.12 2.72 26.95 N. 4\frac{1}{2} W. 22.00 21.93 1.75 East. 16.58 16.58 120.08 32.46 32.24 34.21	Cor. S.	2	က			4	3	
Bearing. Dist. N. S. North. 7.81 7.81 4.32 S. 764 E. 18.15 4.32 S. 103 W. 28.42 27.92 N. 844 W. 27.12 2.72 N. 4½ W. 22.00 21.93 East. 16.58 22.34	W.			5.30	26.98	1.73		34.01
Bearing. Dist. N. North. 7.81 7.81 8.764 E. 18.15 8.103 W. 28.42 8.72 8.72 N. 4½ W. 22.00 21.93 East. 16.58 120.08 32.46 3	ы́		17.63				16.58	
Bearing. Dist. North. 7.81 S. 764 E. 18.15 S. 103 W. 28.42 N. 844 W. 27.12 N. 44 W. 22.00 East. 16.58	vi		4.32	27.92				32.24
Bearing. North. S. 764 E. S. 103 W. N. 844 W. N. 4½ W. East.	N.	7.81			2.72	21.93		32.46
	Dist.	7.81	18.15	28.42		22.00	16.58	120.08
N	Bearing.	North.	S. 764 E.	S. 10\frac{3}{4} W.	N. 844 W.	N. 4½ W.	East,	
	Sta.	-	જ	က	1	ರ	9	

.59900

801.4975 2)1602.9950

Area, 80 A. 0 R. 23.96 P.

PROBLEM 10.

EXAMPLE 2.

S. Areas.				396.7180	1082.2756	1976.6409	3455.6345 1151.2168	2)2304.4177	1152.2088 134.4907	1286.6995	128.66995	2.67980	40	27.19200						e, 59.8800	7.3920	45.0547	24.1040	s, 134.4907	-	
N. Areas.	431.5788	215.3404	504.2976				1151.2168		7.19 P.	•	•	•		•						1st Stat. Line, 59.8800	: 50 re	: 3	4011	Area off-sets, 134.4907		
D. M. D.	17.96	17.96	41.92	65.90	89.89	65.91		-	128 A. 2 R. 27.19 P.		Areas.		12.8100	21.9450	40.1150	11.2395	2)86.1095	43.0547		Areas.		16.6400	22.6920	8.9960	2)48.3280	24.1640
	17.96					29.99			37		Sums.		3.05	5.70	5.65	2.95		-		Sums.		3.25	4.65	5.60		
ᆆ		17.96	00.9	17.98	6.01					3d Stat. Line.	i		4.20	3.85	7.10	3.81		-	4th Stat. Line.		-	5.12	4.88	3.46		
sş.				6.03	12.04	29.99				d Stat	s. Int.			_	_			_	h Sta	Off-sets. Int. Dist.		L				
ż	24.03	11.99	12.03					•		ನ್	Off-sets. Int. Dist.	0.55	2.50	3.20	2.45	0.50		_	4	Off-set	0.50	2.75	1.90	0.70		
or. W.	П	0	0	0	0	П	જ				Dist.	0.00	4.20	8.05	15.15	18.96				Dist.	0.00	5.12	10.00	13.46		
Cor. S. Cor. W.	П	-	0	0	0	П	က				No.		0.5	က	4	5				No.	1	જ	က	4		
.W.	17.95					86.62	47.93	.02 Error W					8	20	28	86	8	8	00			,				
<u>a</u>		17.96	00.9	17.98	0.01		47.95	.02 I			Areas.		23.7900	26.3250	27.7458	34.0992	7.8000	2)119.7600	29.8800		_					
zi.				6.02	12.04	29.98	48.04				Sums.		3.90	6.50	2.06	6.66	3.25	GV.				Areas.		7.3920	7 3990	
z.	24.04	12.00	12.03				48.07	S03		1st Stat. Line.	Int. Dist.		6.10	4.05	3.93	5.12	2.40		-	H	za Stat. Line.	Off-sets.	0.55	0.55		_
Dist.	30.00	21.00	13.44	18.96	13.46	42.41	139.87	Error S.		st Sta	s. Int.			1	1_				_	770	or Star	Dist. Of	0.0			_
ng.	3 W.	E.E.	田田	田田	屈	W.			,		Off-sets.	0.50	3.40	3.10	3.96	2.70	0.55		_			No. Di	0	2 13	-	_
Bearing.	N. 36 ³ W	N. 56½ E.	N. 26\} E.	S. 71₺ E.	S. 26½ E.	S. 45 W.					Dist.	0.00	6.10	10.15	14.08	19.20	21.60				1	Z	1			_
Sta.	-	03	က	4	ړه ا	9		•			No.	-	03	က	4	ಬ	9		_							

PROBLEM 10. (EXAMPLE 3.)

Adding 1' to each of the angles, we find the bearings as follows:

S. Areas.			69.2466	2.4772	71.7238	2)69.6722	34.8361	39.3028	3,93028	3.72112	40	28.8448											
N. Areas.		2,0516			2.0516		Ares. 3 A. 3 B. 28 8448 P.															_	
D. M. D.		2.23	7.86	5.63			3 A. 3 B			Areas.		.1394	.2706	.7820	1.0880	0000	.5250	.3750	2)3.1800	1.5900	2.8767	4.4667	
W. 1				5.63	5.63		Are			Sums.		.41	.41	89.	.68	8.	.25	.25					
E E		2.23	3.40	1112	5.63				On CD.	Int. Dist.		.34	99.	1.15	1.60	.65	2.10	1.50					
s;			8.81	.44	9.25					Off-sets.	0.00	.41	00.	89.	00.	00.	.25	00.					
z.	8.33	26.			9.25					Dist.	0.00	.34	1.00	2.15	3.75	4.40	6.50	8.00	<u> </u>				
Cor. S.	03	0	cs	1	20					<u> </u>	<u> - </u>	<u> </u>	<u> </u>	1			-	1	<u> </u>				
W.				5.63	5.63																		
ā		2.23	3.40		5.63	~*				Areas.		.3500	.3599	.5016	1,8432	.4100	1.9180	.0748	.1003	.0550	.0525	.0882	2)5.7535
αį			8.79	.43	9.55	.05 Error S.				Sums.		.35	19.	.76	96.	1.00	.70	:55	.17	Ħ.	.21	.21	ରି
'n.	8.35	.92			9.27	.05			AB.	i —		<u> </u> 8	.59	99.	1.92		74	.34	.59	.50	.25	.42	
Dist.	8.35	2.41	9.45	5.65					On AB.	Int. 1		1.00		<u> </u>	1.9	7.	2.74	•	***		3.		
ng.		34' E.	ر اجا اجا	.W .6						Off-sets. Int. Dist.	0.00	.35	.26	.50	.46	.54	.16	90.	.11	00.	.21	90.	
Bearing.	N.	N. 67° 34′ E.	S. 21° 8′ E.	S. 85° 39′ W.						Dist.	0.00	1.00	1.59	2.52	4.17	4.58	7.32	2.66	8.25	8.75	9.00	9.43	
Sta.	D	ပ	В	V																•			

PROBLEM 13.

Example 2. (Pl. 2, fig. 5.)

Here the various angles will be found to be as in the following proportions. Then,

L1		,									
To	find log. o	of GA	:								
	As sin. F			,						An Co	0.000140
	Is to sin.										
	So is FG	20 c	h	-	-	-	-	-	-		1.301030
	To GA			-	۰.	-	-	-	-		1.269857
To	find log. (3B+									
10			100							1 - C-	0.154400
	As sin. F										0.174489
	Is to sin. So is FG	GFB	24°	-	-	-	-	•	-		9.609313
	So is FG	-		-	-	-	•	-	-		-1.301030
	To GB			-	-	-	-	-	-		1.084832
To	find log. (20.									
10			00 1 ~!							4 0	0 4 0 44 0 0
	As sin. G	CF 4	3, 12,		•	-	-	-	-	Ar. Co.	0.164193
	Is to sin.	GFC									
	So is FG	· -		_	-				_		1.301030
	To GC			_			-		_		1.254565
											====
T_{0}	find log. (. Ut									
10			4 40 90	, .						A C .	0.154338
	Is to sin.							-	7		9.933066
	So is GF	ہ		-	-	-	-	-	-		1.301030
		e.									
	To GD			-	-	-	-	-	-		1.388434
To	find log.	GE:									
			250 20	,						Ar Co	0.236046
	Is to sin.										9.987832
	So is GI	· -	- 4-	-	-	-	0	-	-		1.301030
											1.504000
	To GE			-	-	-	-	-	-		1.524908

To find 2 ABG:	
As radius Ar.	Co. 0.000000
Is to sin. AGB 91°	9.999934
	1.084832
So is BG, AG $ \begin{cases} BG \\ AG \end{cases} $	- 1.269857
To 2 ABG 226.268	2.354623
To find 2 BGC:	
As radius Ar	Co. 0.000000
Is to sin. BGC 15° 15'	- 9.420007
So is GB, GC \ \ GB	1.084832
So is GB, GC $\begin{cases} GB & \cdots & \cdots \\ GC & \cdots & \cdots \end{cases}$	- 1.254565
To 2 BGC 57.465	1.759404
To find 2 CGD:	
As radius Ar.	Co. 0.000000
Is to sin. CGD 22° 15′	9.578236
So is GC, GD	1.254565
So is GC, GD $ \begin{cases} GC \\ GD \end{cases} $	- 1.388434
To 2 CGD 166.431	2.221235
To find 2 DGE:	
As radius Ar.	Co. 0.000000
Is to sin. DGE 35° 30′	9.763954
So is GD, GE	- 1.388434
(GE	1.524908
To 2 DGE 475.657	2.677296
To find 2 EGA:	
As radius Ar.	Co. 0.000000
Is to sin. EGA 18°	9.489982
So in EC CA (GE · · · ·	1.524908
So is EG, GA $GA - GA - GA - GA - GA - GA - GA - $	1.269857
То 2 ЕGA 192.640	2.284747
2 DGE 475.657	
2 CGD 166.431	
2 BGC 57.465	
892.193	
2 AGB 226.268	
2)665.925	
ABCDE 332.9625 Ch. = 33 A. 1	R. 7.4 P.

CHAPTER IV.

LAYING OUT AND DIVIDING LAND.

PROBLEM 1.

EXAMPLE 2.

Here, 325 Acres = 3250 chains. And side = $\sqrt{3250} = 57 \text{ chains}$.

PROBLEM 2.

EXAMPLE 2.

Here breadth $=\frac{5 \text{ Acres}}{8 \text{ chains}} = \frac{50}{8} = 6.25 \text{ chains.}$

PROBLEM 3.

EXAMPLE 2.

Here, 27 A. 3 R. 20 P. = 4460 P. And, As 7:9::4460:5734.2857. $\sqrt{5734.2857} = 75.725 = \text{length}$. Also, As 9:7::75.725:58.897 = breadth.

PROBLEM 4.

Example 2. (Pl. 2, fig. 6.)

Here, 114 A. 2 R. 33.4 P. = 1147.0875 chains. Also, $\sqrt{1147.0875 + 7.55^2} = \sqrt{1204.09} = 34.7$. And, 34.7+7.55 = 42.25 length. 34.7-7.55 = 27.15 breadth.

PROBLEM 5.

Example 3. (Pl. 2, fig. 7.)
Here, 2 Acres = 320 Perches.

A	n	d	
77	77	u	9

As AB, sin. A	{ AB	30 P A 71° 15′	Ar. Co.	8.522879
So is radius				
To AC 22.53 -				1.352741

Example 4. (Pl. 2, fig. 8.)

As AB, sin. A	AB 32.26 - sin. A 83° 30′	Ar. Co. 8.491336 Ar. Co. 0.002801
Is to ABCD 740		2.869232
So is radius		10.000000
To AD 23.09 -		1.363369

PROBLEM 6.

Example 2. (Pl. 2, fig. 9.)

Here, 27 A. 1R. 16 P. = 273.5 Ch.

63043
00000
46543
09586

PROBLEM 7.

Example 2. (Pl. 2, fig. 10.)

Construction.

Make AB, equal to the greater of the given sides (20). Draw BD perpendicular to AB, equal to twice the given area, divided by AB (12.39). Through D draw DC parallel to AB. Then if AC be made equal to the other given side (16.25), and BC be joined; ABC will be the triangle.

For the Division Line. Make AP = 8.50 the given distance. Take AF to AC in the ratio of the part to be cut off to the whole area. Join PF, draw BG parallel to it; then PG will be the division line.

Demonstration.

AB: AP:: AG: AF, Therefore, AB. AC: AP. AG:: AC. AG: AG. AF:: AC: AF, or AB. AC. sin. A: AP. AG. sin. A:: AC: AF:: m:n (m being the whole area, and n the part to be cut off.) Hence, since AC. AB sin. A = m, AP. AG sin. A = n, and PG is the division line.

Calculation.

As ABC 123.9375	;		 Ar. Co.	7.906798
So is AB.AC	(AB	20 -	 	1.301030
DO IS AD. AC	₹ AC	16.25	 	1.210853
To AP.AG	<u>,</u> 1		 	1.895802
AP = 8.50 -			 	0.929419
AG = 9.255			 	0.966383

PROBLEM 8.

Example 2. (Pl. 2, fig. 11.)

Here, As BAC 100 ch.			
Is to BDG 45			
So is BA ²	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	 	1.397940
To BD ²		 2	2)2.449093
BD = 16.77		 	1.224546

PROBLEM 9.

Example 2. (Pl. 2, fig. 12.)

Here the angles are, A =				
As sin. A. sin. B	sin. A	71° 45′	Ar. Co.	0.022414
As sin. A. sin. b	ight in	49° 15′	66 66	0.120580
In to made aim C	(radius			10.000000
Is to rad. sin. C	sin. C	59° -		9.933066
So is 2 ABC 80 o	ch			1.903090
To AB2				0)1 070150
				<u> </u>
AB = 9.763			·	.989575

PROBLEM 10.

Example 2. (Pl. 2, fig. 13.)

	Here the angles $A=99^{\circ}$ 30', $B=122^{\circ}$, and P	
And.	As sin. A. sin. B $\begin{cases} \sin. A 99^{\circ} 30' & \text{Ar. Co} \\ \sin. B 122^{\circ} & \text{.} \end{cases}$	0.005997
11114,	(sin. B 122° - " "	0.071580
	Is to rad. sin. P { radius	
	(Sill. 1 41 90	
	So is 2 ABCD 50 ch	- 1.698970
	To fourth term 39.61	- 1.597812
	AB^2 36	===
	$CD^2 - \sqrt{75.61} = 8.695.$	
	$CD^2 - \sqrt{75.61} = 8.695.$	
Also,	As sin. P 41° 30′ Ar. Co	0.178735
		- 9.928420
	So is DC—AB 2.695	- 0.430559
	To AD 3.449	- 0.537714
		-
	TI 0 (TN 0 (*)	
	Example 3. (Pl. 3, fig. 1.)	
H	lere the angles are, $A = 90^{\circ}$, $B = 73^{\circ}$ 30', and	$P = 16^{\circ} 30^{\circ}$.
4.1	sin. A 90° - Ar. Co	0.000000
Also,	As sin. A. sin. B $\{\sin B 73^{\circ} 30' - \text{``} \text{``} \}$	0.018263
	(radius	- 10.000000
	Is to radsin. P sin. P 16° 30′	- 9.453342
	So is 2 ABCD 160 ch	- 2.204120
	To fourth term 47.39	- 1.675725
	AB ² - 182.25	======
	$CD = \sqrt{134.86} = 11.61.$	÷
And,	As sin. P 16° 30′ Ar. Co	0.546658
	Is to sin. B 73° 30′	9.981737
	So is AB—CD 1.89	0.276462
	To AD 6.38	0.804857

PROBLEM 12.

Example 2. (Pl. 3, fig. 6.)

Here, As $2:1::BC^2(100):EF^2=50$,

 $EF = \sqrt{50} = 7.07.$

And, As BC (10): EF (7.07):: AB (15): AF = 10.605.

PROBLEM 13.

Example 2. (Pl. 3, fig. 7.)

Here the angles are, $A=36^{\circ}~30',~B=100^{\circ}~30',~C=43^{\circ},~E=74^{\circ}~30',$ and $F=69^{\circ}.$

As sin. E. sin. F Is to sin. C. sin. B So is BC ²	\{ \sin. E 74° 30 \\ \sin. F 69 \\ \sin. C 43° \\ \sin. B 100° 30' \\ \{ BC \}	 9.992666 1.270912
To fourth term 259.	54 4	 2.414210
$9)\overline{1038}$ $EF = \sqrt{115}$		
As sin. A 36° 30′ Is to sin. E 74° 30 So is EF 10.74 - To AF 17.40 -)′ 、	

PROBLEM 14.

Example 2. (Pl. 3, fig. 8.)

Here, EF = $\sqrt{\left(\frac{AB^2 + CD^2}{2}\right)}$ = $\sqrt{5796.18}$ = 76.13. And, DC—AB (29.4): FE—AB (16.13) :: AD (30) : AF = 16.46

PROBLEM 16.

EXAMPLE 1. (Pl. 3, fig. 12.)

The area of this tract may be found to be 858.552 square chains. (The latitudes and departures are mostly given in the subsequent operations.)

To find area ABCDE, and the latitude and departure of EA.

	N.	S.	E.	w.	D. M. D.	N. Areas.	S. Areas.
AB		9.15		6.46	40.86		373.8690
BC	17.21			17.20	17.20	296.0120	
CD	10.41		2.89		2.89	30.0849	
DE		3.61	15.60		21.38		77.1818
EA		(14.86)	(5.17)		42.15		626.3490
	27.62	27.62	23.66	23.66		326.0969	1077.3998 326.0969
						2 ABCDEI	751.3029 858.552
							2)107.2491
						AEI	53.6245

							,
	N.	S.	E.	w.	D. M. D.	N. Areas.	S. Areas.
AE	14.86			5.17	5.17	76.8262	
EF	.93		21.49		21.49	19.9857	
FA		(15.79)		(16.32)	26.66		420.9614
				,		96.8119	96.8119
							2)324.1495
						AEF	162.07475
As AEF 162.07475 Ar. Co. 7.790285							
	Is to A	EI 53	$.6245 \cdot$			1.	729363
1	So is l	at. EF	.93			—1.9	968483
	To lat.	EI .3	1 -			1.	488131

As AEF	-	-	-	-	Ar. Co.	7.790285
Is to AEI	-	-	-	-		1.729363
So is depart. EF 21.49	-	-	-	-		1.332236
To depart. EI 7.11	-	-	-	-		0.851884

	N.	S.	E.	w.
AE	14.86			5.17
EI	.31		7.11	
IA		(15.17)		(1.94)

										8.819014
Is to de	part.	1.94	4 -	-	-	-	-	-		0.287802
So is ra	dius	-		-	-	-	-	-		10.000000
To tang	. bear	ring	ΑI	7°	17′	-	-	-		9.106816
As cos.	bear	ing		-	-	~	-	-	Ar. Co.	0.003518
										10.000000
So is di	ff. lat	t. 15	.17	-	-	-	-	-		1.180986
To dist.	ΑI	15.29	9 -	-	-	-	-	-		1.184504

- CHAPTER V.

MISCELLANEOUS QUESTIONS.

Question 1.

Here $\frac{1}{2}$ Acre = 2420 square yards; And radius = $\sqrt{\left(\frac{2420}{3.1416}\right)}$ = $\sqrt{770.3081}$ = 27.75.

QUESTION 2.

Construction.

Make AB (Pl. 4, fig. 1) = 40 = one of the given sides, and at A draw AL perpendicular to AB and = $\frac{320}{40}$ = 8; through L draw GH parallel to AB, and with the centre A and distance = 20 = the other given side, describe an arc, cutting GH in D and C; join AC, BC, AD, and BD: then will ABC and ABD answer the conditions of the question.

Calculation.

AE = AF = $\sqrt{AC^2 - CE^2} = \sqrt{400 - 64} = 18.3303$; and BE = AB—AE = 21.6697; therefore, BC= $\sqrt{BE^2 + EC^2} = \sqrt{533.57589809}$ = 23.099. Also, BF = AB+AF=58.3303, and BD = $\sqrt{BF^2 + FD^2}$ = $\sqrt{3466.42389809} = 58.876$.

Another Solution.

Find AE = AF as before. Then, from Geometry, BC² = AB² + AC² - 2 AB.AE = 2000 - 1466.424 = 533.576, and BC = 23.099. Also, BD² = AB² + AD² + 2 AB.AF = 2000 + 1466.424 = 3466.424, and BF = 58.876.

QUESTION 3.

Here it is evident the number of acres will be inversely as the number of square yards in a Perch:

Therefore, $6^2:5.5^2::110 \text{ A.}:92 \text{ A.} 1 \text{ R.} 28\frac{3}{9} \text{ P.}$ Cheshire. And $7^2:5.5^2::110 \text{ A.}:67 \text{ A.} 3 \text{ R.} 25\frac{15}{49} \text{ P.}$ Irish.

QUESTION 4.

Here $\frac{28}{12} = \frac{7}{3} =$ twice the thickness of the wall, also 840 links = 554.4 feet=the longer diameter within the walls; 612 links=403.92 feet = the shorter; $554.4 + \frac{7}{3} = \frac{1670.2}{3} =$ longer diameter outside, and $403.92 + \frac{7}{3} = \frac{1218.76}{3} =$ shorter. By Prob. 10, Chap. III. the area within the walls = $554.4 \times 403.92 \times .7854 = 223933.248 \times .7854 =$ 175877.1729792 ft. = 4 A. 0 R. 6 P. The area to the outside = $\frac{1670.2}{3} \times \frac{1218.76}{3} \times .7854 = \frac{2035572.952}{9} \times .7854 = \frac{1598738.9965008}{9} = 177637.6662778$ feet. Therefore 177637.666 — 175877.173 = 1760.493 = area the wall stands upon.

QUESTION 5.

Here the area of an ellipse whose diameters are 3 and 2 is 4.7124. Then, since similar figures are as the squares of their like dimensions, we have, As 4.7124:160::9:305.5768 = square of the longer diameter; consequently $\sqrt{305.5768} = 17.481 = \text{longer}$ diameter; and 3:2::17.481:11.654 = shorter diameter.

QUESTION 6.

Find the area of the triangle whose sides are 9, 8, and 6; thus, $\frac{9+8+6}{2}=11.5$, and $\sqrt{11.5\times2.5\times3.5\times5.5}=\sqrt{553.4375}=23.525$ square perches. Also, 6 A. 1 R. 12 P. = 1012 P., and 23.525: 1012 :: 8²: 2753.1562 = square of the second side; therefore $\sqrt{2753.1562}=52.47$. Also,

8:9::52.47:59.029 = longest side. 8:6::52.47:39.353 = shortest side.

To find ABC:	uestion '	7. (Pl.	4,	fig.	2.)			
AB	27.35								
BC	31.15								
CA	38.00								
OA.									
	2)96.50								
Half sum	48.25	-	-	-	-	-	-	- '	1.683497
	(20.90	-	-	-	-	-	-	-	1.320146
Remainders	} 17.10	-	-	-	-	-	-	-	1.232996
	(10.25	-	-	-	-	-	-	-	1.010724
									2)5.247363
ABC 420.417									${2.623681}$
ABC 420.417		-	-	-	•	-	-	-	====
To find ACE:									
AC	38.								
CE	40.10								
EA	22.20								
	2)100.30								
Half sum	50.15	-	-	-	-	-	-	-	1.700271
	(12.15	-	_	_	-	-	-	-	1.084576
Remainders	$\left. \begin{array}{c} 10.05 \end{array} \right.$	-	-	-	-	-	-	-	1.002166
	(27.95	-	-	-	-	-	-	-	1.446382
									2)5.233395
ACE 413.71		-	-	-	-	-	-	-	2.616697
To find CED:									
CE	40.10								
$^{\mathrm{CD}}$	23.70								
DE	29.25								
	2)93.05								
Half sum	46.525								1.667686
ALL OUT DOLLAR	(6.425	_		-	_		-		0.807873
Remainders	22.825	_	-	-					1.358410
	(17.275	-	-	-	-	-		-	1.237408
									$2)\overline{5.071377}$
CED 343.311		-	-		-	-	-	-	2.535688

Hence the whole area = 420.418+413.71+343.308 = 1177.436 Ch. = 117 A. 2 R. 38.976 P.

QUESTION 8.

Construction.

Make AB (Pl. 4, fig. 3.) equal to half the given perimeter = 52, and bisect it in D; make DC perpendicular to AB and equal to the square root of the given area; with the centre C and radius equal to AD, describe an arc cutting AB in E, complete the rectangle AEFG and it will be the one required. The demonstration is evident from Geometry.

Calculation.

DE =
$$\sqrt{\text{CE}^2-\text{CD}^2}$$
 = $\sqrt{676-480}$ = $\sqrt{196}$ = 14.
AE = AD+DE = $26+14$ = 40, and EF = EB = $26-14$ = 12.

QUESTION 9.

Construction.

Draw any line AC, (Pl. 4, fig. 4.) and in it take AE = 20 = given difference; make EF perpendicular to AC = 20; join AF and produce it to B, making FB = 20; then will AB be a side of the square.

Demonstration.

Since EA = EF, the angles FAE and AFE are each equal to half a right angle, and AC must be the diagonal of the square. Again the triangles CEF and CBF are equal, since they are right angled at E and B, and have the hypothenuse and one leg in each equal: we have therefore CE = CB = CA—20.

Calculation.

 $AF = \sqrt{AE^2 + EF^2} = \sqrt{800} = 28.284$, and AB = AF + FB = 48.284; hence the area = $AB^2 = 2331.344656$ sq. per. = 14 A. 2 R. 11.34 P.

QUESTION 10.

Construction.

Let ABCD (Pl. 4, fig. 5.) be the given rectangle. In BA and BA produced take BH = BC, and AR = \frac{3}{4} AD. On BR describe the semicircle BPR, meeting DA produced in P; bisect AH in O, and with the centre O and radius OP, describe the semicircle EPQ, make AG = AQ, complete the rectangle AF, and the thing is done.

Demonstration.

 $AF = AE \times AG = AE \times AQ = AP^2 = AB \times AR = \frac{3}{4}AB \times AD = \frac{3}{4}AC$. Also, BE = BH—HE = BC—AQ = AD—AG = GD.

Calculation.

AO = $\frac{1}{2}$ AH = 10: AP² = AB× $\frac{3}{4}$ AD = 6000; therefore, OP = $\sqrt{\text{AP}^2 + \text{OA}^2}$ = $\sqrt{6100}$ = 78.1025; BE = BO—OE = 90—78.1025 = 11.8975.

QUESTION 11.

Construction.

Let ABD (Pl. 4, fig. 6.) be the given circle. Draw the diameter AB and radius CD perpendicular to it; take CF = 4 AC; upon BF describe a semicircle cutting CD in E: with C as a centre and radius CE, describe the circle EGH, and the thing is done.

Demonstration.

CE is a mean proportional between CF and CB; hence CF: CB:: $CE^2:CB^2::4:5$; and since circles are as the squares of their radii, we have $GEH = \frac{4}{5}ABD$.

Calculation.

$$\sqrt{5}: \sqrt{4}:: AC (75): EC = \frac{75\sqrt{4}}{\sqrt{5}}$$

= $\frac{150\sqrt{5}}{5} = 30\sqrt{5} = 67.082$, and DE = DC—EC = 7.918.

QUESTION 12.

Construction.

With the given distances form the triangle ABC, (Pl. 4, fig. 7.) Upon AB describe the equilateral triangle ABD; join CD and on it describe the equilateral triangle CDE, which will be the one required.

Demonstration.

Since BD and BC are by construction two of the given distances; it is only necessary to prove that BE = AC, which is evident from the equality of the triangles DAC and DBE.

Calculation.

In the triangle	ABC, find	the angle	BAC, thus,
-----------------	-----------	-----------	------------

BC	10												
AC	7.5	-	-	-	-	-	-	-	-	A	r. (Co.	9.124939
AB	12.5		-	-	-	-	-	-	-	A	r. (Co.	8.903090
	2)30.												
	15	-	-		-	-	-		_		-	-	1.176091
	5	-		-	-	-	-	-	•	-	-	-	0.698970
												2)	19.903090
Cos.	½ BAC				26°	34'	,	-	-	-	-	-	9.951545
	BAC				53°	8'							

Then in the triangle DAC we have DA and AC, and the angle DAC = 113° 8' to find DC, thus,

As DA+AC 20	-		-	Ar. Co.	8.698970
Is to DA— Λ C 5	-		-		0.698970
So is tang. $\frac{DCA + ADC}{2}$	-	33° 26′	-		9.819684
To tang. $\frac{DCA-ADC}{2}$	-	9° 22′	-		9.217624
ACD	-	42° 48′			
And,					
As sin. ACD 42° 48′	-		-	Ar. Co.	0.167848
Is to sin. DAC 113° 8'	,		-	,-	9.963596
So is AD 12.5			-		1.096910
To DC 16.92	-		-		1.228354

Then in CDE, we have the sides and angles to find the area thus,

As radius		-	-	-	-	Ar.	Co.	0.000000
Is to sin CDE								
So is CD > DE	∫ CD	-	-	-	•	-		1.228354
So is CD×DE	. (DE	-	-	-	-	-		1.228354
To 2 CDE	•							
	193 94 (h	1	12 4	١.	1 R	23.0	4 P

QUESTION 13.

Construction.

With the given bearings and distances protract the figure ABCDfg Pl. 4, fig. 8. Join Ag, and with the centres g and A, and distances equal to the 4th and 7th sides, describe arcs cutting in G. Join AG and gG, and draw DE, EF, and FG respectively parallel and equal to gG, Df, and fg. Then will ABCDEFG be the required map.

Calculation.

To find the bearing and distance of gA.

	Bearing.	Dist.	N.	s.	E.	W.
AB	S. 72 W.	24.00		7.42		22.83
BC	North.	38.00	38.00			
CD	N. 82½ E.	41.00	5.35		40.65	
Df	S. 80 E.	11.50		2.00	11.32	
fg	S. 26 W.	22.00		19.77		9.64
gA				(14.16)		(19.50)
			43.35	43.35	51.97	51.97
Is S	s diff. lat. 14.1 s to departure of is radius - to tang. bearing as cos. bearing s to radius - to is diff. lat. 14 to distance gA 2	19.50	 4° 1′ W.	Ar.	- 1.290 - 10.000 - 10.138 - 10.000	0035 0000 8972 === 0955 0000 1063

In the triangle AGg we have the sides to find the angles AgG and GAg;

0,						
Thus,						
AG	37					
gG	20	Ar.	Co.		8.698970	
Āģ	24.1	Ar.	Co.		8.617982	
	2)81.1					
Half sum	40.55			-	1.607991	
Remainder	3.55			-	0.550228	
				2)	19.475171	
Cos. $\frac{1}{2}$ AgG	56° 52	<u>1</u> ' -		-	9.737585	
m AgG	113° 45′	_				
And,						
As AG 37 -				-	Ar. Co.	8.431798
Is to gG 20				_		1.301030
So is sin. AgG	113° 45′		-	-		9.961569
To sin. gAG 2	29° 39′ -			-		9.694397

Applying now the bearing of gA to these angles we will have the bearing of gG or DE = S. 59° 44′ E, and of GA = S. 83° 40′ W The area will then be calculated as in the following table, viz.

	IVI I	. 5 U	шы	LA.	NE	00	5 Q	UES
S. Areas.	169.6267			993.6864	254.3600	2548.8508	333.0576	4299.5815 217.0710
N. Areas.			217.0710		t			
D. M. D.	22.83	00.00	40.65	98.58	127.18	128.86	82.44	
W.	22.83					9.64	36.78	
Е.			40.65	17.28	11.32			
vi	7.43			10.08	2.00	19.78	4.04	
Ŋ.		37.99	5.34					
Cor. S. Cor.W.								
Cor. S.	-	1	-			-	-	
W.	22.83					9.64	36.78	69.25 69.25
E.			40.65	17.28	11.32			1
vi	7.42			10.08	2.00	19.77	4.03	43.30
z.		38.00	5.35					43.35
Dist.	24.00	38.00	41.00	20.00	11.50	22.00	37.00	
Bearing.	S. 72 W.	North.	N. 82½ E.	S. 59\frac{3}{4} E.	S. 80 E.	S. 26 W.	S. 833 W.	
Sta.	AB	BC	CD	DE	EF	FG	GA	

4)511.25 P. 40)2041.2553

2)4082.5105

Area, 12 A. 3 R. 1.25 P.

QUESTION 14.

Construction.

Make AB, (Pl. 4, fig. 9.) = the given side, and divide it in D, so that AD may be to DB in the ratio of 3 to 2; in AB produced, take DO a fourth proportional to AD—DB, DB, and AD, and with the centre O and radius OD, describe the semicircle DCE; make AG perpendicular to AB, and equal to twice the area divided by AB = 6; through G draw GF parallel to AB, cutting the circle in C and F; join AC BC, AF and BF; then will ABC and ABF answer the conditions of the question.

Demonstration.

Since AD—DB: DB:: AD: DO, we have AD: DB:: AO: DO or AO: AD:: DO: DB, therefore, AO: DO:: DO: OB, consequently (Euclid, F. 6.) AC: BC:: AD: DB:: 3:2; and AF: BF: AD: DB:: 3:2.

Calculation.

As 3+2:15::3:AD=9, and DB = 6; also, 9-6:6:9:DO=18, and AO = 9+18=27, join OC, and OF, and let fall the perpendiculars CL and FP; then OL = $\sqrt{OC^2-CL^2}=\sqrt{324-36}=\sqrt{288}=16.9706$, and AL = AO-OL = 10.0294; hence AC = $\sqrt{AL^2+LC^2}=\sqrt{136.5886436}=11.6871$; and as 3:2::11.6871: BC = 7.7914. Again AP = AO+OP = 43.9706, and AF = $\sqrt{AP^2+PF^2}=\sqrt{1969.41366436}=44.3781$; and as 3:2::44.3781: BF = 29.5854

Question 15. Construction.

Make AB, (Pl. 4, fig. 10.) = the given side, and BL = the sum of the other sides; Bisect AB in D, and take DH a third proportional to 2 AB and BL; Draw HE perpendicular to BH and equal to $\frac{1600}{50} = 32$. Through E draw EF parallel and equal to BL; join EA and produce it to G, making FG = AB; draw AC parallel to FG, and join BC; then ABC is the triangle required.

Demonstration.

By Construction $BL^2 = 2 AB \times DH$; also, in the similar triangles EGF and EAC, we have GF (AB): AC:: EF (BL): EC (HP).

And

Hence $BL \times AC = GF \times HP$, or $2BL \times AC = 2GF \times HP$. Subtracting these equals from the preceding, we have $BL^2-2BL\times AC=$ $2 AB \times DH - 2 GF \times HP = 2 AB \times DP = (BP + AP) \times (BP - AP) =$ BP^2 — AP^2 = BC^2 — AC^2 . Hence BL^2 — $2BL \times AC + AC^2$ = BC^2 , and BL - AC = BC, or BL = BC + AC.

Calculation.

As 2 AB (100) : BL (85) :: BL (85) : DH = 72.25, and AH = DH-AD=47.25. Now in the right angled triangle AHE, we have the sides AH and HE, to find HAE and AE; thus,

	As AH 47.25									
	Is to HE 32 -	-	-	-	-	-	-	-		1.505150
	So is radius -	-	-	-	-	-	-	-		10.000000
	To tang. HAE	34°	61	ī'	-	- ,	-	-	-	9.830748
l,										
	As cos. HAE 34									
	Is to radius									
	So is AH	-	-	-	-	-	-	-		1.674402
	To AE 57.07									1 756282

Now in the triangle GEF we have FE, FG, and the angle FEG = HAE, to find FGE; thus,

As FG 50	-	-	-	·-	Ar. Co.	8.301030
Is to FE 85	-	-	-	-		1.929419
So is sin. GEF $34^{\circ} 6\frac{1}{2}'$	-	-	-	~		9.748776
To sin. FGE 72° 25' -	-	-	-	-	:	9.979225

Finally, in ACE we have AE and the angles to find AC; thus,

As sin. ACE $73^{\circ} 28\frac{1}{2}'$		-	-	-	-	Ar. Co.	0.018319
Is to sin. AEC 34° $6\frac{1}{2}$ ′	-	- `	-	_	-		9.748776
So is AE	-	-	-	-	-		1.756383

To AC 33.3793 -1.523478

And BC = 85 - 33.3793 = 51.6207.

Question 16.

Construction.

Make AC (Pl.4, fig. 11.) = 50 = the given diagonal, and on it describe a semicircle ABC; make AE perpendicular to AC and = $\frac{1200}{50}$ = 24; draw EB parallel to AC, cutting the semicircle in B; join AB, BC, and draw CD and DA parallel to them; then will ABCD be the rectangle required.

Demonstration.

Since ABC is an angle in a semicircie, it is right, and ABCD is a rectangle. Also its area = $AC \times BF = 1200$ perches = $7\frac{1}{2}$ acres.

Calculation.

FG = $\sqrt{BG^2 - BF^2}$ = $\sqrt{49} = 7$; AF = AG-GF = 18, and AB = $\sqrt{AF^2 + FB^2}$ = $\sqrt{900} = 30$, BC = $\sqrt{AC^2 - AB^2}$ = $\sqrt{1600} = 40$.

Question 17.

Construction.

Make AB (Pl. 4, fig. 12.) = the square root of the given area, and draw CE perpendicular to it: draw BC, making ABC = 30°, make AE = AC; bisect AC in D, and draw EF perpendicular to CE and = ED. Complete the parallelogram CEFG, which will be the one required.

Demonstration.

Since the angle B = 30°, and A = 90°, BC = 2 AC = CE = 4 CD, and EF = ED = 3 CD; therefore FC = $\sqrt{EF^2 + EC^2}$ = 5 CD. Also AB² = BC² — AC² = $\frac{3}{4}$ BC² = $\frac{3}{4}$ EC² = EC × ED = EC × EF = CEFG.

Calculation.

Since $AB^2 = \frac{3}{4}CE'$ $CE^2 = \frac{4}{3}AB^2 = \frac{4}{3}$ the given area = 784, and CE = 28; hence $EF : \frac{3}{4}EC = 21$.

Question 18.

Construction.

With the given bearings and distances protract the figure ABCD, (Pl. 4, fig. 13.) and from B draw BP according to the given bearing

and distance of the spring. Produce DA and CB to meet in F, and through P draw EH parallel to AD. Bisect AF in G, join EG, and draw BM parallel to it, and MN parallel to FE. Make MT perpendicular to MN, and equal to the square root of the given area. Take MU a third proportional to MN and MT; draw UH parallel to MN, cutting AF in I; draw IK perpendicular to AF and equal to EP, and with the centre K and distance PH describe an arc cutting AD in Q; draw QPR, and the thing is done.

Demonstration.

In the similar triangles FGE and FMB, we have FB: FM: FE: FG; therefore, 15.6, the triangle EFM=BFG; but EFM= $\frac{1}{2}$ FMNE, and BFG= $\frac{1}{2}$ BFA; hence FMNE=BFA. Again, because the triangles EPR, IQS, and PHS are similar, and the homologous sides EP (IK), IQ, and PH (KQ) form a right angled triangle, we have from Geometry EPR+IQS=SPH. Add FISPE to each, and we have FQR=EFIH. But FBA=EFMN, hence BAQR=MNIH=MN.MU=MT²=the given area.

Calculation.

From the bearings of the lines the angles may be found as follow. AFB = BEP = 23° , ABF = 84° 30′, BAF = 72° 30′, EBP = 145° 30′, and EPB = 11° 30′. Then, in the triangle EBP we have all the angles and side BP, to find EP and EB:

Thus,	
As sin. BEP 23° Ar. Co	0.408122
Is to sin. EBP 145° 30′	9.753128
So is BP 7.90	0.897627
To EP 11.452	1.058877
And,	
As sin. BEP Ar. Co.	0.408122
Is to sin. BPE 11° 30′	9.299655
So is BP	0.897627
To BE 4.031	0.605404

Also, in the triangle	ABF, all the	angles and	side AB	are given,
to find BF and AF;				

o ma m	and	AI 5													
Thus,															
As s	in. A	FB s	23°	-	-	-	-	-	-	-	A	r. C	o.	0.4081	22
Is to	sin.	BAF	72	2° 5	30'	-	-	-	-	-	-	-	-	9.9794	20
So is	s AB	15.2	0	•	-	-	-	-	-	-	-	-	•	1.1818	44
То	BF	37.1	01	-	-	-	-	-	-	-	-	-	-	1.5693	86
And,															
As s	in. A	FB	-	-	-	-	-	-	-	-	Ar	: C	o.		
Is to	sin.	ABF	84	t° {	30'	-	-	-	-	-	-	-	-	9.9979	
So is	s AB	•		-	-	٠	-	-	-	-	-	-	-	1.1818	44
To	AF	38.7	22	-	-	-	-	-	-	-	-	-	-	1.5879	62
And	FE:	= FB	I	3E		33.0	7,	and	F	G =	$=\frac{1}{2}$	ΑF	' =	19.361	;
Also,							ĺ				Ī				
As I	EF 3	3.07	-	-	-	-	-	-	-	-	Aı	: C	o.	8.4805	66
Is to	GF	19.3	61	-	-	-	-	-	_	-	-	_	-	1.2869	27
So is	s BF	37.1	01	-	-	-	-	-	-	-	-	-	-	1.5693	86
To I	FM :	21.72	1	-	-	-		-	-	-	-	-	-	1.3368	7 9
Now, in	n the	naral	امام	orre	am	M	тн	N -	OVA	har	υ _ρ .	MN	J	FE —	33.07
and IMN															
Thus,			,							Z (I o		011		,	101 1,111,
I IIus,					(MN	1 2	3 U.	7		Δν	· C	۱۵	8.4805	see
As I	MN,	sin. I	MN	[- (MN						0.4081	
Te to	radi	ine -	_	_	,	21110	- 11		_	_		_		10.0000	
	s MI											_		2.0000	
	MI 7	-,									_	_		$\frac{2.0000}{0.8886}$	
101		.,50												====	=

a

Therefore PH = EH - EP = FM + MI - EP = 18.008. Now, in the right angled triangle IKQ, we have IK = EP = 11.452, and KQ = PH = 18.008, to find IQ; thus,

Hence AQ = FQ - FA = FM + MI + IQ - FA = 4.636.

QUESTION 19.

Construction.

With the given bearings and distances, protract the figure ABCD, (Pl. 4, fig. 14;) then, by Prob. 15, Chap. IV. divide ABCD into two equal parts by the line EF, parallel to CD; also, by the same problem, divide ABCD, and EBAF, each into two equal parts by the lines OM and PN, parallel to AD; join MN, produce it to I, and draw OH parallel to IM; join IH, then will EF and IH be the division lines required.

Demonstration.

Because PN is parallel to OM, we have IN: NM:: IP: PO: IG: GH, because NG is parallel to HM; therefore, PG is parallel to OH, and consequently to IM. Now since OH is parallel to IM, we have IHM = IOM, to each add AIMD, and AIHD = AOMD = $\frac{1}{2}$ ABCD. In the same manner it may be shown that AIGF = $\frac{1}{2}$ ABEF = $\frac{1}{4}$ ABCD.

Calculation.

Draw EK and IL, each parallel to AD, and MU parallel to AB. From the given bearings find the angle $A=78^{\circ}~30',~B=139^{\circ}~45',~C=78^{\circ}~45',~and~D=63^{\circ}.$ By Prob. 15, Chap. IV., find EF and AF, thus,

As sin. C. sin. D	{ sin. C 78° 45′ sin. D 63° -	Ar. Co.	0.008426
Is to sin. A. sin. B	\sin. A 78° 30' - \sin. B 139° 45'		
So is AB ²	(AB 23 AB		1.361728
00 IS 1 LD	(AB		1.361728
To fourth term	383.274		2.583510
$\mathrm{CD^2}$	2161.3201		
2)	2544.5941		
$\mathbf{EF} = \mathbf{V}$	$\overline{1272.2970} = 35.67$		

And in the triangle ECK,	
	0.208243
Is to sin. C 78° 45'	- 9.991574
So is CD—EF 10.82	1.034227
То FD - 17.14	- 1.234044
AD · 49.64	
AF 32.50	
Then in the triangle ECK, we have the angles ar FD, to find EC, thus,	nd side EK =
As sin. C 78° 45' Ar. Co.	0.008426
Is to sin. K 63°	9.949881
So is EK 17.14	1.234044
To CE 15.57	1.192351
Consequently $BE = BC - CE = 14.93$. Now by the blem find OM, AO, PN and AP, thus, $A = \frac{1}{2} - \frac{1}{2} - \frac{1}{2} = \frac{1}{2} - \frac{1}{2}$	·
As sin. A sin. D $\begin{cases} \sin A - \frac{1}{2} & AI = 0.5 \\ \sin D - \frac{1}{2} & AI = 0.5 \end{cases}$	
(sin B	9.810316
Is to sin. B. sin. C sin. C	9.991574
(BC 30.50	1. 484300
So is BC^2 BC	1.4 84300
To fourth term 675.18 AD ² 2464.1296	2.829416
2)3139.3096	
$OM = \sqrt{1569.6548} = 39.62$	
And,	
As sin. RMD 38° 30′ Ar. Co.	0.205850
Iș to sin. D	9.949881
So is AD—OM 10.02	1.000868
To AO 14.34	1.156599

And,							
As sin. A. sin. F	{ sin. sin.		-				0.008807 0.050119
Is to sin. B.sin. E	{ sin. }		-	-	-		9.810316 9.991574
So is BE ²	-	14.9	3	-	-		1.174060 1.174060
To Fourth term	16	31.7 8	-	-	-		2.208936
AF ²	- 10	56.25					
	2)121	18.03					
PN	√60	9.01	= 24	4.68	3.		
And,							
As sin. RMD 38° 3 Is to sin. F So is AF—PN 7				-	Ar. -	Co.	0.205850 9.949881 0.893207
To AP 11.19 -			-	-	-		1.048938
Hence $OP = AO -$	– AP =	= 3.13	5; W	vhe:	refo	re we	e have
OM—PN (14.94) : PN (3 AP—IP = 5.99.							
In the triangle MUL we $MU = IO = IP + PO = 8.5$							
As sin. ULM 63°					Ar	. Co.	0.050119
Is to sin. MUL 78	30'			-			9.991193
So is MU 8.35 -		·	-	-	-		0.921686
To ML 9.18			-	-	-		0.962998
And,							
As sin. MLU 63°		-			Ar	Co.	0.050119
Is to sin. UML 38	30'		•	-	-		9.794150
So is MU 8.35 -			-	•	-		0.921686
To UL 5.83		• -	•	-	-	• •	0.765955

Therefore IL = IU + UL = OM + UL = 45.45, and from the similar triangles ILM and OMH, we have

As IL
$$(45.45)$$
: LM (9.18) :: OM (39.62) : MH = 8.

Now, in the triangle ILH, we have the angle L=D, and sides IL and LH=LM+MH=17.18, to find the angle LIH; thus,

As LI+LH 62.63 -	-		-	-	Ar.	Co.	8.203218
Is to LI — LH 28.27							
So is tang. $\frac{LHI + LIH}{2}$	-	58°	30′	•		-	10.212681
To tang. $\frac{LHI-LIH}{2}$							
LIH		22	7				
Bearing IL -	•	66	15				
" IK -	S	. 88	22	E.			

